

1 Winterization of Texan power system
2 infrastructure is profitable but risky

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10 **Abstract**

11 We deliver the first analysis of the 2021 cold spell in Texas which com-
12 bines temperature dependent load estimates with temperature dependent
13 estimates of power plant outages to understand the frequency of loss of
14 load events, using a 71 year long time series of climate data. The expected
15 avoided loss from full winterization is 11.74bn\$ over a 30 years investment
16 period. We find that large-scale winterization, in particular of gas infras-
17 tructure and gas power plants, would be profitable, as related costs for
18 winterization are substantially lower. At the same moment, the necessary
19 investments involve risk due to the low-frequency of events – the 2021
20 event was the largest and we observe only 8 other similar ones in the set
21 of 71 simulated years. Regulatory measures may therefore be necessary
22 to enforce winterization.

23 **Keywords**— Texas, extreme event, power systems, winterization

24 Weather extremes such as storms can significantly affect the reliability of power
25 systems [1]. The increasing use of variable renewable energies additionally exposes
26 power systems to hazards caused by weather extremes [2, 3]. However, recently it was
27 a gas power dominated system which was deeply impaired by a weather extreme: a cold
28 spell over Texas, between February 10th and February 20th, 2021 with temperatures far
29 below 0° caused a failure of large parts of the Texan power system. The combination
30 of extraordinarily high winter electricity demand and more importantly the failure of
31 significant power generation capacities, both due to low temperatures, resulted in up
32 to 4.5 millions of Texans being cut-off from their electricity supply [4].

33 Wu et al. [5] provide an open source grid simulation to conduct a very detailed
34 analysis of the 2021 event, but do not put the 2021 event into a long-term climatic
35 context. In contrast, Doss-Gollin et al. [6] have shown that lower temperatures than
36 in February 2021 have been observed in the past 71 years, and heating demand pre-
37 dicted from temperature data would also have been higher in the past, although the

38 2021 frost event was comparably long. There is therefore a striking gap between the
39 occurrence probability of such an event, its large scale economic and social cost, and
40 the lack in winterization efforts. Hence, we assess here how avoided loss due to win-
41 terization compares to its cost. We do so in a simulation framework which allows to
42 estimate the probability distribution of loss of load events, thus being able to derive
43 the uncertainty of the magnitude of avoided loss within the investment period. Tech-
44 nically, we combine estimates of temperature dependent load with a model of power
45 plant outages, taking into account 71 years (1950–2021) of past climate from reanalysis
46 data. Climate change, of course, may have an impact on temperatures. We therefore
47 also assess if trends in the occurrence of extremely cold temperatures and loss of load
48 events can be observed. Furthermore we conduct an extensive sensitivity analysis to
49 show uncertainties arising from our modelling choices.

50 What happened in February 2021?

51 Starting on 10th of February 2021, temperatures in Texas began to fall, causing load to
52 increase from around 40 GW to over 70 GW by February 14th–15th. On February 15th
53 the aggravating frost reached a critical level where substantial shares of generation
54 capacities began to fail. Available capacities dropped below demand leading to a
55 sustained power generation capacity deficit (Figure 1). Consequently, rolling blackouts
56 had to be implemented to stabilize the grid and prices at the power market increased
57 to the upper limit of 9000\$/MWh. The deficit event continued until 20th February
58 when rising temperatures allowed the system to recover.

59 The highest load forecast in the February 2021 event was well above the highest
60 load observed in winter in the period 2004–2020¹. Our estimate is in the range of
61 observed extreme summer loads (see Appendix Figure A.1). In contrast, ERCOT
62 forecasts of peak load during the cold spell have been higher by about 4GW compared
63 to our estimates [10], indicating an almost record-high predicted load on the network.
64 Our estimates therefore have to be considered to be conservative.

65 Besides leading to high electricity load, the low temperatures also caused substan-
66 tial outages of generation capacities. Gas capacity failures were responsible for the
67 largest share in power outages. Out of 62GW of thermal capacity expected to be
68 available in winter by ERCOT², 25.4GW of thermal capacity failed in total, with the
69 share of gas being 20.1GW. Based on the predicted demand and the observed load,
70 we estimate that in total 1.19TWh of load were affected by blackouts. The maximum
71 total outage capacity, including wind power, was 44.4GW, causing 24GW of peak lost
72 load, when using our load prediction model. Loss of load occurred in 107 hours in the
73 period from 2021-02-15 02:00 to 2021-02-19 12:00 local time.

74 Outages of gas generation capacities started to increase rapidly at a gas power
75 plant weighted temperature of -8.8°C, which is a record low temperature compared to
76 the past 17 years (see Figure A.2). The outages were not only related to freezing of
77 power plants, but also of gas supply infrastructure, including gas production equipment

¹The values of loss of load and load prediction in this section rely on our simulation and may therefore differ from ERCOT reports to some extent. Served load and plant outages are taken from ERCOT. As we focus on estimating the long-term frequency of such events, we did not aim at reproducing the February 2021 model in highest detail.

²Actual capacity available before the event has been higher, but transient stability requirements and reactive power demands have reduced the amount of load that has been covered in the system [5]

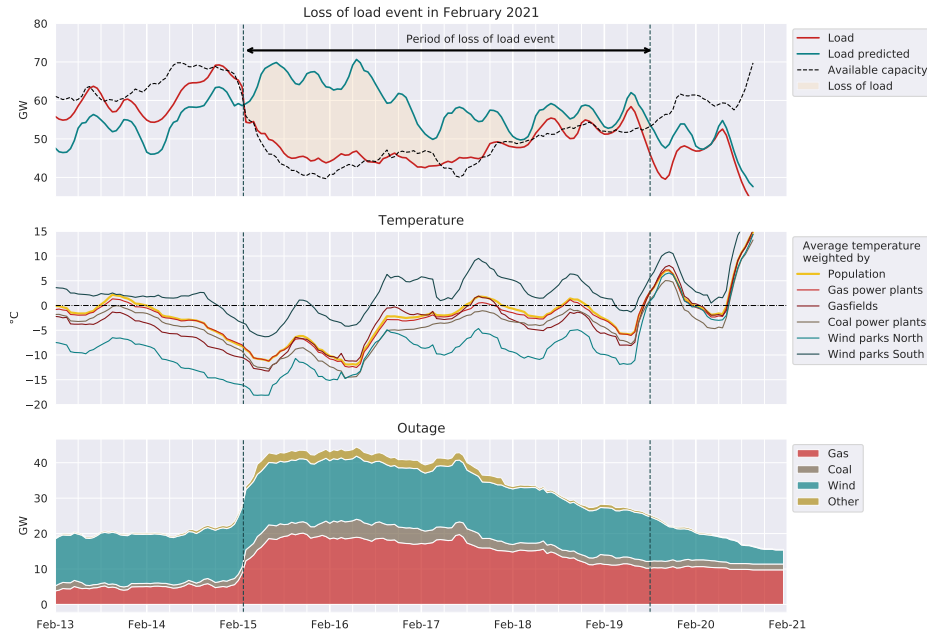


Figure 1: Observed load, predicted load, available capacity, temperatures and outages during the February 2021 event (based on ERCOT load and outages [7, 8], ERA5 temperatures [9], and our load prediction model combining the two)

78 at gas fields. Power plants started failing rapidly when temperature weighted by gas
 79 fields dropped below -10.9°C . In the period 2004–2021, when no other outage events
 80 comparable to the one in 2021 was observed, this is a record low gas field weighted
 81 temperature (see Figure A.2). Therefore, gas supply infrastructure may have played
 82 an important role in the outage events. This is confirmed by ERCOT, which classified
 83 around 8GW of outages being related to limited fuel supply [11].

84 Coal generation capacity came offline at average temperatures weighted by coal
 85 plant locations of below -10.2°C . This temperature is at the very lower end of the
 86 temperature distribution in the period 2004–2020. For both technologies, coal and
 87 gas, recovery time was substantial. Even when temperatures recovered back to over
 88 0°C , 11.3GW of thermal power plants, i.e. 18% of total available thermal capacity,
 89 stayed offline for another 16 hours.

90 Temperatures weighted by wind power plant locations indicate that the failure
 91 of wind power plants may be a more frequent event. While temperatures at wind
 92 parks in Southern Texas were at the very lower end of the temperature range observed
 93 in the period 2004–2020, the average wind park temperature in Northern Texas was
 94 just below 0°C and well within the range of previously observed low temperatures.
 95 Compared to thermal power generation, wind power capacities began to fail much
 96 earlier and at higher temperatures. On February 13th, when gas outages summed up
 97 to only 5GW, ERCOT already reports 13GW of wind power outages (Figure 1).

98 How extreme was the February 2021 event?

99 Our simulations of loss of load events using climate data from 71 years shows that
100 the 2021 event was a record one³. In total, we estimate that eight other severe power
101 deficit events would have occurred in the current system assuming climate from the
102 period 1950-2021 (see Figure 2). The second largest power deficit event at 0.98 TWh
103 is predicted when using climate data from 1989.

104 In our model predictions, the loss of load event has a duration of 107 hours, and
105 causes an aggregated deficit of 1.39TWh, at a peak capacity deficit of 25.9GW. There
106 are several events with similar peak capacity deficits identified in the 1950–2001 period,
107 but none of the events has a comparably long duration and a comparably high amount
108 of loss of load (Figure 2). 1989 was the last time a similar frost event occurred. This
109 long break in frost events of a significant magnitude may explain why the recent event
110 hit an insufficiently winterized power production system.

111 The 2021 record high loss of load is not caused by the frost magnitude alone but
112 by a combination of a long, relatively cold frost event and an inopportune timing
113 of the frost peak. According to Figure 1 the system failure occurred early and was
114 prolonged by a long frost period afterwards. This is in contrast to other years when
115 temperatures recovered more quickly after temperature minima had been reached (e.g.
116 in 1951 and 1963). This finding is supported by the extreme value statistics of the
117 frost spells shown in Figure A.3. 2021 was the longest frost event in seven decades. It
118 has a return period of 141 years. Other events, however, were colder (1951, 1989) or
119 had higher frost sums (1951).

120 In terms of load, the highest predicted winter load in 2021 was slightly higher than
121 the highest predicted winter load in the complete 71 year time series (Figure A.1),
122 although temperatures were lower in the 1989 event. A particular combination of time
123 of day, day of week, and low temperature caused this particularly high load in 2021.

124 It may also have been expected that frost events would have decreased due to
125 global warming. However, our analysis does not show any significant trend in the
126 loss of load time series (Figure A.9). Still, average temperatures in Texas significantly
127 increased due to climate change since 1951 (Figure A.10). This result is confirmed
128 by others, however, the increase in mean temperature is not genuinely transferable
129 to extreme temperatures [12]. A stratified analysis of annual frost events (minimum
130 annual temperature) below temperature thresholds from 0 to -10 °C reveals that there
131 is indeed no significant observed change of severe frost events below -2 °C (Section
132 A.7). Only very mild frost events showed a significant attenuation (2.6 °C over the
133 past seven decades), but such events are irrelevant for frost related failures of the
134 power system comparable to the 2021 event.

135 Overall, extreme value statistics show that the event of 2021 was severe because
136 of its long frost duration and its frost dynamics. Against the background of seven
137 decades of observed climate data, the frost event had to be expected, especially as we
138 could not find evidence for a decrease of severe frost events due to climate change.
139 This suggests that similar events comparable to the one in 2021 have to be expected
140 again and need to be mitigated even in a future, warmer climate.

³Please observe that the results on the 2021 event in this section differ slightly from the previous section, as we used simulated plant outages instead of outages provided by ERCOT here.

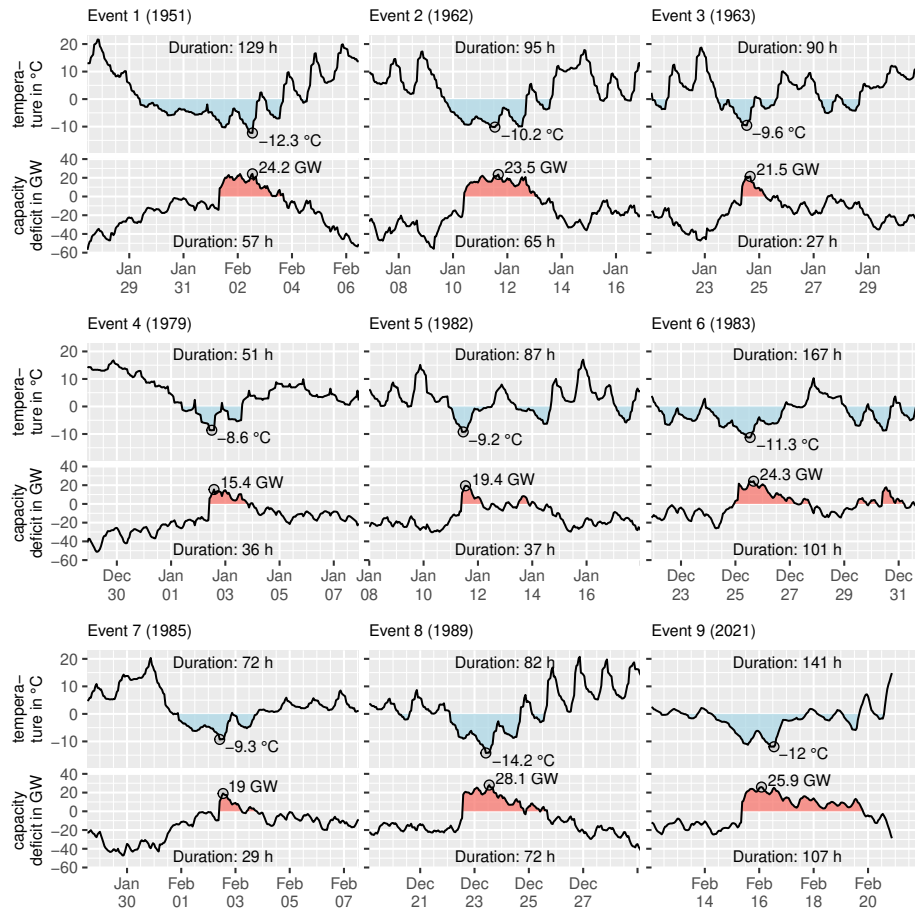


Figure 2: Population weighted temperature and predicted capacity deficit of severe frost events within the 1950-2021 period. Labels in the graph refer to temperature minima and deficit maxima

141 Comparing avoided loss to costs of winterization

142 A bootstrap of loss of load events from our 71 years of simulated capacity deficits yields
 143 an expected loss of load due to a cold weather event in a typical 30 year investment
 144 period of 2.55TWh with a 68% confidence interval of [1.09TWh, 4.02TWh]⁴. The
 145 current maximum market price regulated by ERCOT is 9 000\$/MWh [13]. The avoided
 146 loss for electricity consumers under full winterization is therefore 11.74bn\$ at a 5%
 147 discount rate⁵.

⁴This confidence interval is a result of bootstrapping different loss of load events from different weather years and does not take into account other model uncertainties.

⁵We emphasize here that this loss does not represent full societal cost of load shedding. However, the value is an indicator of incentives to winterize in the system.

148 Expected marginal avoided loss is higher than winterization cost for most of the
149 failed gas, wind, and coal power infrastructure (Figure 3). For the first winterized
150 GW of gas power capacity, expected marginal avoided loss over a 30 years period is at
151 0.98bn\$/GW, but drops to 0.52bn\$/GW at 11GW of winterization. Marginal avoided
152 loss for coal power plant winterization is slightly lower per GW, and significantly lower
153 for wind power. For all technologies, the spread of the marginal avoided loss is high:
154 The 68% confidence interval is at double or half of the expected marginal avoided loss.
155 In 1.7% of all cases, there is no deficit event in a 30 year period, which is the worst
156 case scenario in case of investment in winterization, because there is no avoided loss.

157 Significant winterization measures can be implemented under our estimates of
158 expected marginal avoided loss. In particular, we estimate that the winterization
159 of gas wells in combination with winterization of gas power plants will cost about
160 450M\$/GW (see section A.8). This cost is below the marginal avoided loss up to
161 the 13th GW of winterized capacity. Winterization of coal and wind power plants
162 is significantly cheaper, as fuel supply infrastructure does not have to be winterized.
163 Winterization costs assumed at 10% of initial plant investments of coal power plants
164 are far below marginal avoided loss up to full winterization of all failed coal capacity. In
165 fact, one could even assume winterization cost of 30% of initial plant investments and
166 winterization cost would still be lower than the marginal avoided loss for the completely
167 winterized capacity. For wind turbines, our estimates of marginal avoided loss are half
168 those of coal, but are still substantially higher than the costs of winterization which
169 are reported to be 5% of investment costs [14].

170 How reliable are our estimates?

171 Estimates of loss of load events depend mainly on the assumptions on outage tem-
172 peratures for gas power plants, as their failure has by far the biggest impact on the
173 magnitude of loss of load events. An increase in outage temperatures from -8.8°C
174 to -5.8°C increases loss of load from 6.04–6.48TWh to 12.61–13.18TWh in 71 years,
175 depending on the respective recovery temperature (see Figure 4). In contrast, the
176 outage temperatures assumed for wind and coal power plants have a minor impact
177 on the estimates of loss of load, if they are changed for one technology only (in the
178 range of 5.67–6.34TWh). A concurrent increase of outage temperatures of all power
179 generation technologies changes loss of load from 5.92–6.54TWh to 15.92–16.94TWh
180 when increasing the outage temperature by 3°C . In contrast, recovery temperatures
181 do not change our estimates of loss of load significantly, as loss of load shows less than
182 1TWh difference within a variation of outage temperature of 3°C . Lowering outage
183 temperatures decreases our estimates likewise. For a temperature decrease of 3°C , the
184 loss of load predictions are less than a third of our base estimate (1.61–1.90TWh).

185 Our finding that 2021 was the largest simulated loss of load event in the period
186 1950–2021 is sensitive to the assumed outage temperature. If outage temperatures of
187 power plants are simultaneously increased by 1.5°C , 2021 becomes the second largest
188 event while 1983 becomes the largest event. If additionally the recovery temperature
189 falls by 1.5°C , 2021 becomes the third largest event, as 1983 and 1989 are larger. The
190 loss of load event in 2021, however, in none of the sensitivity simulations has a rank
191 lower than 3 in terms of total loss of load.

192 While it is certain that climate change affects average temperatures, our analysis
193 indicates that it may not have caused a trend of decreasing extreme cold events. Nev-
194 ertheless, we assessed how the number and magnitude of power deficit events would

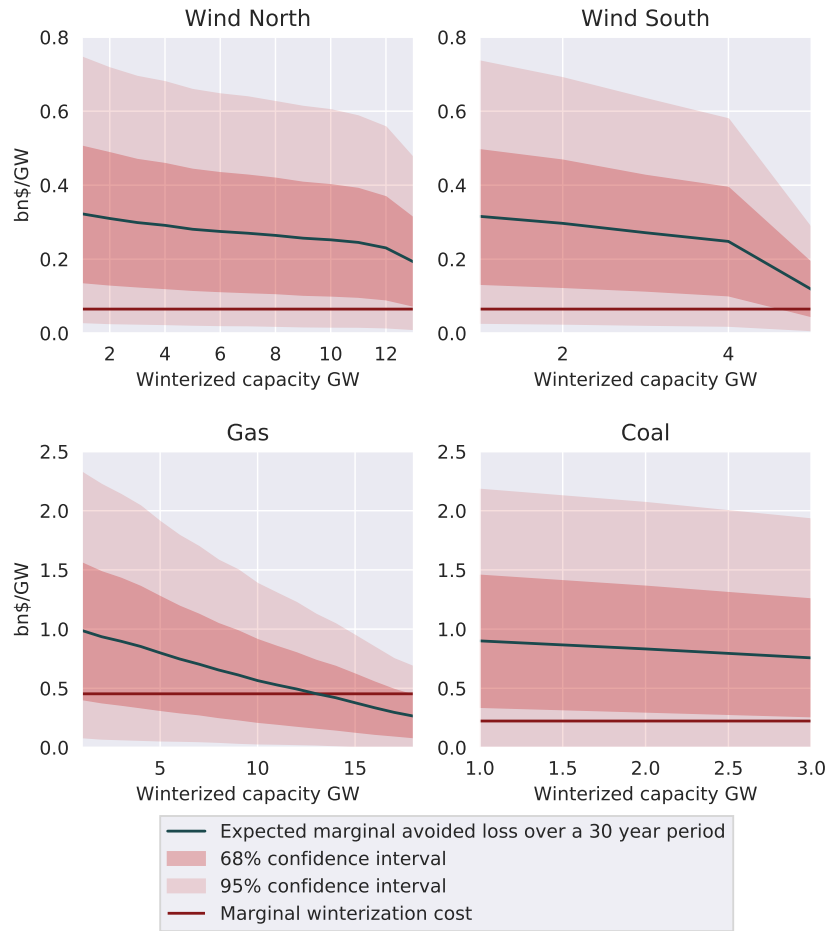


Figure 3: Comparison of marginal avoided loss (bn\$/GW of winterized capacity in a 30 year period) to marginal costs for winterizing existing power generation capacity

195 change if temperature extremes would follow the same trend as average temperature.
 196 Under such assumptions, we find that the number of severe loss of load events is
 197 reduced from 9 to 8, while the loss of load drops from 6.11TWh to 4.37TWh and
 198 3.66TWh, assuming 2021 and 2050 as years for simulation, respectively (see section
 199 A.7 for modeling details). We emphasize here that our approach is in contrast to
 200 observations (see A.5) and should only be understood as sensitivity analysis. Never-
 201 theless, even under such a scenario, the loss of load is still significant and - a however
 202 reduced - extent of winterization would be profitable.

203 Instead of using aggregated outage curves by technology, as we do in our analysis,
 204 we have also developed plant level outage curves. When using those, the number
 205 of events increases from 9 to 48, however, the total deficit increases from 6.11TWh

206 to 9.72TWh only, as most events are minor. Such a high number of outage events
 207 is unrealistic, as they were not observed in the period 2004–2021, for which data
 208 is available. We conclude that at the moment the used outage data provided by
 209 ERCOT does not allow to derive temperature dependent plant level outages that
 210 represent reasonable loss of load events. Our aggregated approach also is associated
 211 with significant uncertainty (see A.4), but is more consistent with observed real world
 212 loss of load events.

213 Estimating the avoided loss from full winterization without using the 2021 event
 214 decreases slightly our estimates from 11.74bn\$ to 9.24bn\$. However, winterization of
 215 coal and wind is still highly profitable, and the corresponding winterized capacity for
 216 gas power is only 4GW lower than in a scenario including 2021. This indicates that
 217 even before the occurrence of the 2021 event, significant loss of load events had to be
 218 expected.

219 Finally, the assumed discount rate has a significant impact on results. When
 220 increasing the rate from 5% to 7%, the avoided loss under full winterization is reduced
 221 from 11.74bn\$ to 9.74bn\$. While winterization of coal and wind power still fully pays
 222 off under these assumptions due to low winterization cost, the profitable winterization
 223 of gas infrastructure and gas power is reduced from 13GW to 10GW.

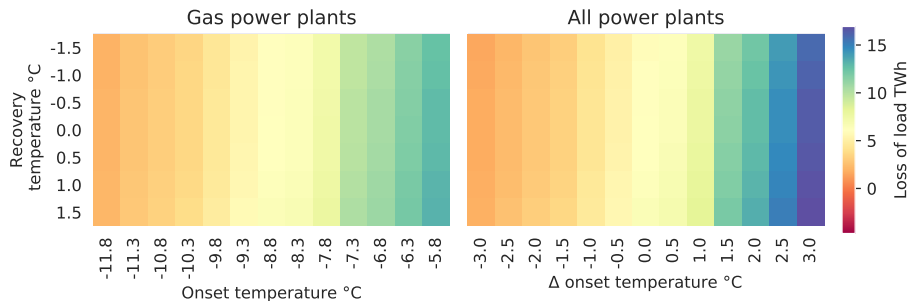


Figure 4: Sensitivity of the accumulated loss of load between 1950 and 2021 by generation type to onset temperature and recovery temperature used in the outage model for a variation of gas threshold temperatures (left) or all threshold temperatures together (right)

224 Discussion

225 We have shown that the Texas loss of load event in February 2021 was among the
 226 top three extreme events when simulating the power generation system under climate
 227 conditions of the last 71 years. In particular winterization of gas power plant and gas
 228 supply infrastructure is crucial to prevent future events.

229 Our analysis indicates that events of significant loss of load had and have to be
 230 expected, which make considerable winterization efforts profitable on average. How-
 231 ever, we have also shown that significant risk is associated with such investments, as
 232 the spread of avoided loss implies high uncertainty. Furthermore, our estimates of
 233 avoided loss are based on the price cap in the electricity market. The incentives of
 234 different actors in the power system to avoid that loss will depend on their long and

235 short position in the market. Due to both, high risk and a somehow complex incentive
 236 structure, we see the need for regulatory intervention to enforce winterization. Apart
 237 from winterization, other flexibility measures, in particular strong demand response
 238 measures and an expansion of transmission capacities to neighbouring states, may be
 239 beneficial for the system not only during cold spells, but also to make the system
 240 more stable during the ongoing transition to a larger share of renewable energies in
 241 the power generation mix.

242 In a broader societal perspective the actual costs of load shedding to society, in
 243 particular during catastrophic, long-lasting events, may not be represented by the
 244 regulated price cap. This implies that benefits from winterization may even be signifi-
 245 cantly higher than our analysis indicates. Higher estimates for the value of lost load
 246 can be found in literature [15] and others have determined the costs to society implied
 247 by the 2021 event in Texas being an magnitude of order higher than ERCOT’s price
 248 cap [5].

249 Of course, our results have to be considered in the light of a continuously evolving
 250 power system. We assume 30 years of lifetime for all installed capacities, however some
 251 capacities may soon be retired and their winterization may not be profitable therefore.
 252 As winterization of new capacity is cheaper and easier to implement than winterization
 253 of existing one, winterization standards for installing new power plants and associated
 254 infrastructure should have high priority. The ongoing transformation of the Texan
 255 power system can therefore be considered an opportunity to ensure robustness during
 256 future cold events.

257 Methods

258 We use a chain of statistical and simulation models to derive loss of load events, and
 259 expected avoided loss from winterization⁶. The data sets which feed the models and
 260 model interactions are shown in Figure 5. A detailed explanation of all involved mod-
 261 els and data sets is given below.

262 **Estimation of temperature induced electricity deficits:** To estimate the
 263 amount of deficits in the power system, we simulate the difference between the ex-
 264 pected, temperature dependent electricity demand and the available generation ca-
 265 pacity.
 266

267 Formally this can be described by defining the capacity deficit $d_{y,h}$ as the difference
 268 between the demand $_{y,h}$ and the available generation capacity $c_{y,h}$ in year y in hour of
 269 year h :

$$d_{y,h} = \text{demand}_{y,h} - c_{y,h} \quad (1)$$

270 The total loss of load d_y^{tot} in a year is the sum over $d_{y,h}$ for all hours where capacity
 271 deficit was larger than 0:

$$d_y^{\text{tot}} = \sum_{\substack{h, \\ \text{demand}_{y,h} \geq c_{y,h}}} d_{y,h} \quad (2)$$

⁶Code related to this analysis will be available upon final publication at <https://github.com/inwe-boku/texas-power-outages>

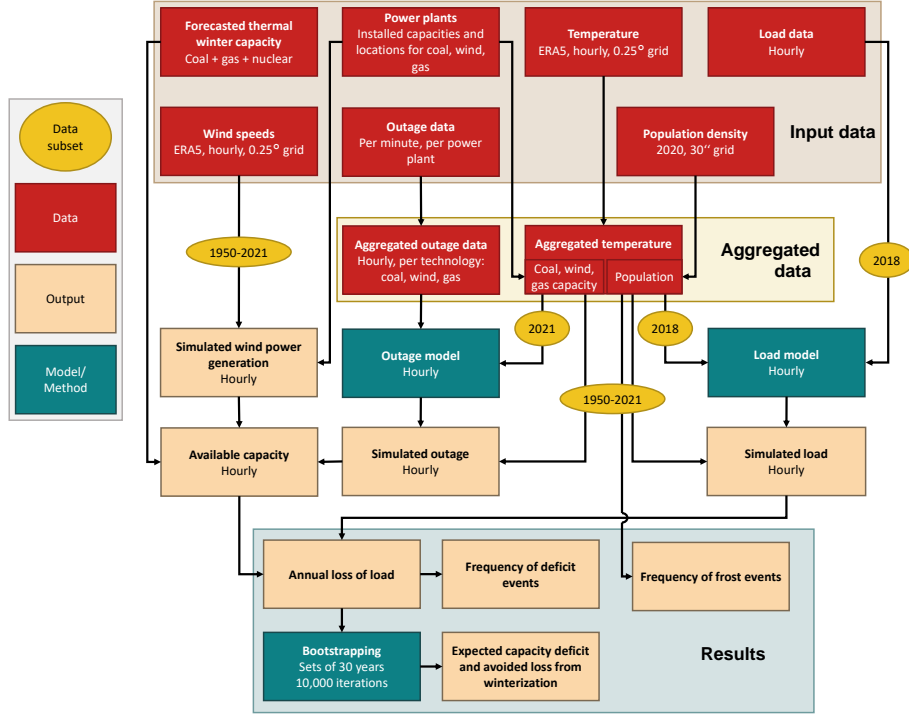


Figure 5: Overview of data inputs and deficit model

272 Demand is simulated from load in the past using a linear regression model. Avail-
 273 able generation capacity is obtained by reducing the total available capacity by tem-
 274 perature dependent outages:

$$c_{y,h} = c^{\text{thermal}} - o_{y,h}^{\text{gas}} - o_{y,h}^{\text{coal}} + w_{y,h} \frac{c^{\text{wind}} - o_{y,h}^{\text{wind}}}{c^{\text{wind}}} \quad (3)$$

275 where c^{thermal} is the total available thermal capacity in winter according to ER-
 276 COT, and $o_{y,h}^{\text{gas}}$, $o_{y,h}^{\text{coal}}$ and $o_{y,h}^{\text{wind}}$ are the temperature dependent power plant outages,
 277 respectively. Current wind power generation $w_{y,h}$, simulated from wind speeds as-
 278 suming full capacity, is reduced to the share of working wind power capacity, i.e. the
 279 difference between installed capacity c^{wind} and wind power outages $o_{y,h}^{\text{wind}}$, divided by
 280 total installed capacity. We do not model nuclear and solar PV outages, as their over-
 281 all generation capacity and their contribution to outages was low (Figure 1). We also
 282 neglect transmission of power from neighbouring states, which is of minor magnitude.

283 According to ERCOT [16], 67.5GW of capacity was available during the 2021 win-
 284 ter, but 5GW of these may have been under maintenance. We therefore assume a
 285 value of 62GW for c^{thermal} to match our simulation with available capacity during the
 286 event, as indicated by served load.

287

288 **Demand prediction:** We predict demand $_{y,h}$ from temperatures using a regres-

289 sion model (equation (4)). For each year y in the period 2018–2020 we estimate a
 290 model for demand in winter (December–February, the three coldest months on aver-
 291 age), taking into account seasonality (sine and cosine terms depending on the hour of
 292 the year h), and the temperature $t_{y,h}$. Furthermore, we include dummy variables for
 293 the hour of day $\delta_{i,y,h}^{\text{hod}}$, the weekdays $\delta_{i,y,h}^{\text{dow}}$, and for holidays $\delta_{y,h}^{\text{hold}}$. We include $t_{y,h}^4$ into
 294 the equation as with falling temperatures, load shows a highly non-linear increase. We
 295 tested a quadratic, a cubic and a quartic term and the regression with the quartic
 296 term showed the highest fit.

$$\text{demand}_{y,h} = \beta_0 + \sum_{i=1}^7 \beta_i \delta_{i,y,h}^{\text{dow}} + \sum_{j=8}^{31} \beta_j \delta_{j,y,h}^{\text{hod}} + \beta_{32} \delta_{y,h}^{\text{hold}} + \beta_{33} \sin\left(\frac{2\pi h}{8760}\right) + \beta_{34} \cos\left(\frac{2\pi h}{8760}\right) + \beta_{35} t_{y,h} + \beta_{36} t_{y,h}^4 \quad (4)$$

297 We applied the models estimated with data from the years 2018, 2019 and 2020,
 298 respectively, to 2021. The total load differs by a maximum of 2% in the three years.
 299 When predicting with the models for January 2021, the 2020 model shows the highest
 300 fit (RMSE 1.75GW, R^2 0.87, 2019: RMSE 2.31, R^2 0.77, 2020: RMSE 2.96, R^2 0.62).
 301 However, using the 2019 and 2020 model substantially and consistently underestimates
 302 loads at very low temperatures. This is probably due to relatively warm winters in
 303 these years. The 2018 model performs better under these conditions, although load
 304 estimates are still lower than observed at the lower temperature end (Figure 6). In
 305 particular in 2021, all three models underestimate the load in the hours before the
 306 blackouts, although temperatures weren't record low during this time. This warrants
 307 further research.

308

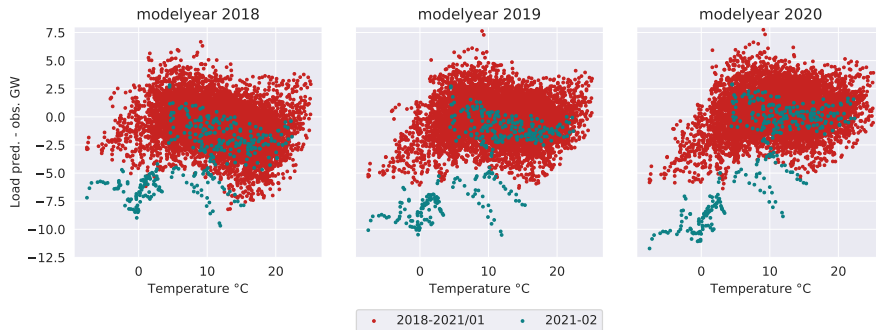


Figure 6: Difference between predicted and observed load applying the regression model estimated from 2018, 2019 and 2020 data to the period 2018–2021/01 and the days before the blackout (2021/Feb/01–2021/Feb/14)

309 **Temperature dependent generator outages:** The power plant outages in
 310 Texas were caused by a systemic failure, as a substantial amount of capacity tripped
 311 in a short period of time [11]. Most of the capacity failed due to weather events, but
 312 the lack of fuel supply was also relevant. Additionally, non- weather related equipment

313 failures and, to a smaller amount, frequency problems in the grid caused problems at
 314 generation units. This implies that temperature at single power plants alone cannot
 315 fully explain outages. We derived infrastructure fragility curves [17] from our data
 316 and they show that 25% of gas power plants, about 30% of wind power plants, and
 317 50% of coal power plants failed when temperatures were above 0°C and in many cases
 318 have not been below 0°C in the days before failure. Other weather conditions besides
 319 freezing temperatures may be partly responsible, but at least wind conditions at the
 320 time of failure were not particularly extreme. Besides freezing temperatures, which
 321 caused failure of power plant components and of gas production and gas distribution,
 322 there are also systemic reasons for failure therefore.

323 We do not use infrastructure fragility curves for modeling outages, but estimate
 324 threshold temperatures and outage capacities during catastrophic failure by technol-
 325 ogy: we derive the temperature, at which the largest increase in outages occurred, from
 326 the 2021 outage data. Furthermore, we estimate an outage level in terms of tripping
 327 capacity. Finally, we also define a constant recovery rate, which describes how outages
 328 decreased after the recovery temperature is reached. This is an aggregate approach
 329 and will omit smaller outages, but it accounts better for the inter-dependency of fail-
 330 ures. A detailed outline of how we derived the outage parameters from the 2021 data
 331 in Texas is given in section A.4. The resulting outage models are subsequently applied
 332 to the 71 years of climate data to obtain capacity availability during this period. In
 333 a sensitivity analysis, we have also tested how loss of load changes if a similar outage
 334 model on the level of individual plants is used instead.

335
 336 **Estimating avoid loss of winterization:** We use the price cap of 9 000\$/MWh
 337 regulated by ERCOT [4] as estimate of the value of lost load. We first derive the loss
 338 of load $d_{y,p,w}^{\text{tot}}$ for different scenarios, where a capacity w of power plants of technology
 339 p (gas, coal or wind in North or South Texas) are winterized. This is done similar to
 340 equation (2) but the maximum outage level for a technology in the outage functions
 341 $o_{y,h}^p$ used in equation (3) is reduced by w . We estimate total loss of load $d_{y,p,w}^{\text{tot}}$ using
 342 temperature data of all years in the period 1950–2021. We combine temperature
 343 dependent demand estimates, simulated wind power generation for the same years
 344 from ERA5 reanalysis wind speeds (for further details see [18]), and the temperature
 345 dependent power plant outage functions for that purpose. The 71 different weather
 346 years therefore serve as a set of different weather realisations where we bootstrap
 347 from. We assume that the power system is equivalent to today’s system. For each
 348 bootstrapping iteration b , we sample 30 years of lost loads $d_{i,b,p,w}^{\text{boot}}$ for $i = 1, \dots, 30$
 349 from the set of $d_{y,p,w}^{\text{tot}}$, $y = 1950, \dots, 2021$. This is done for 10 000 iterations, $b =$
 350 $1, \dots, 10\,000$. Subsequently, total economic loss $l_{b,p,w}$ over a typical investment period
 351 of 30 years is calculated, as shown in equation (5), $r = 0.05$ being the discount rate:

$$l_{b,p,w} = 9\,000 \sum_{i=1}^{30} d_{i,b,p,w}^{\text{boot}} (1+r)^{-i} \quad (5)$$

352 This results in 10 000 different samples $l_{b,p,w}$, allowing to derive a distribution of
 353 economic losses under different scenarios of winterization. To calculate avoided loss
 354 from winterization by technology p , we derive $l_{b,p,w}^{\text{avoid}}$ in the following way:

$$l_{b,p,w}^{\text{avoid}} = l_{b,p,0} - l_{b,p,w} \quad (6)$$

355 We eventually take the first differences of $l_{b,p,w}^{\text{avoid}}$ to derive the marginal avoided loss

356 from winterization.

357

358 **Frequency analysis of frost and power deficit events:** The frequency analysis
359 of extreme events follows well-established methods of hydrological drought analysis
360 [19], where deficit events are defined as periods when the variable of interest is below
361 a certain threshold. Here, we use two different threshold concepts. First, we analyse
362 temperature, and define a constant threshold of 0°C to define deficit events in analogy
363 to drought events in drought statistics. Deficit events in the power system, resulting
364 from low temperatures, are simply defined for periods when the capacity deficit $>$
365 0GW (equation (1)). In each case, the result is a derived deficit time series, which is
366 further investigated using Yevjevich’s theory of runs [20]. During a frost period, minor
367 thaw episodes or other disturbances may split an event in several smaller events. As a
368 remedy, pooling procedures have been recommended [21]. In this study, an inter-event
369 time criterion of 1 day is used to define the deficit event series. In case that multiple
370 events occur in a year the event with the absolutely largest accumulated deficit is used
371 for further analysis. The series so derived are characterized by three deficit charac-
372 teristics: duration (measured in hours), intensity (minimum temperature / maximum
373 power deficit), and severity (aggregated frost sum / power deficit over the event), each
374 of which constitutes an annual extreme value series. These are further analyzed us-
375 ing extreme value statistics to determine the return period of each frost and capacity
376 deficit characteristic according to natural hazard management standards. Our analy-
377 sis was conducted using the R-software package `lfstat` [22], which provides a collection
378 of state-of-the-art methods that are fully described in the World Meteorological Or-
379 ganization’s manual on low flow estimation and prediction [23]. The resulting winter
380 power deficit events are shown in Figure 2, their extreme value statistics are shown in
381 Figure A.3.

382

383 **Data:** Temperature at 2m above ground is taken from the ERA5 reanalysis [9].
384 We weight temperature over Texas by population density [24] to derive a temperature
385 index for modeling electricity demand. For estimating outages in the power system
386 due to low temperatures, we also weight temperature by capacities of wind [25], coal
387 and natural gas power plants [26], which were the power generation technologies most
388 affected by failure during the extreme temperature event of February 2021. For wind
389 power plants, we split into a North and South region (along the latitude of 30°),
390 since temperatures at wind parks in the North and South of Texas differ substantially.
391 Since the failure of the power system might be related to infrastructure at gas fields
392 supplying these power plants [27], we also determine a gas field weighted temperature
393 index, using the distribution of natural gas production by county [28] to complement
394 our analysis. Load data used for demand prediction were retrieved from ERCOT [7]
395 for the period 2004–2021/02. Since the focus of this study is on cold events in winter,
396 only winter load data (Dec–Feb) is used. Outage data is provided in the period since
397 10^{th} of February 2021 by ERCOT [8] and is aggregated by power generation technology
398 for the analysis.

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402 tions of power plant outages and discussed early results with us.

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516 **A Appendix**

517 **A.1 Load and temperature extremes**

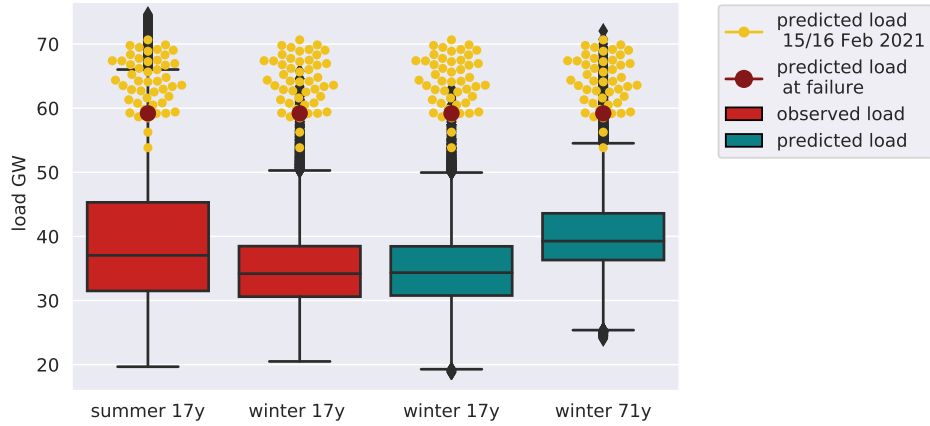


Figure A.1: Observed loads for 17 years (2004–2021/01) for winter (Dec–Feb) and summer (Mar–Nov) periods, predicted winter loads for 17 years (2004–2021/01) and 71 years (1950–2021/01) and extreme loads on February 15th and 16th 2021

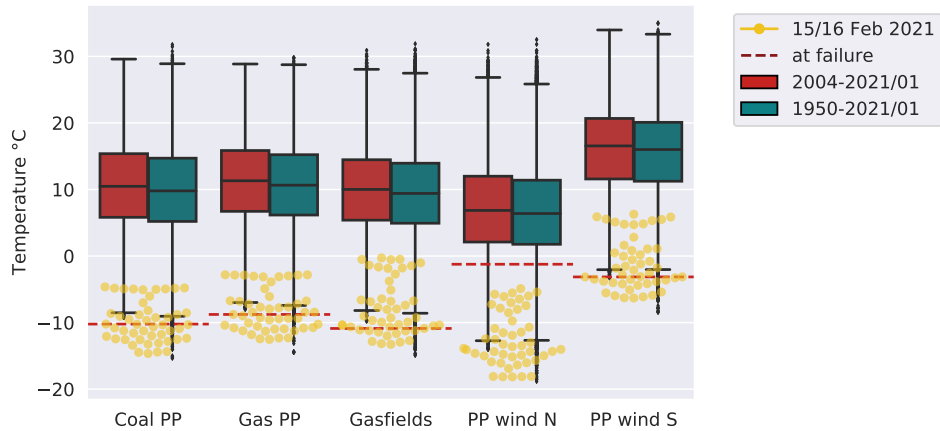


Figure A.2: Winter temperatures weighted by natural gas and power plant capacity, gas field production and wind power plant capacity in North and South Texas compared to temperatures during the 15/16 Feb 2021 event

518
519

A.2 Extreme value statistics of temperature and power deficits

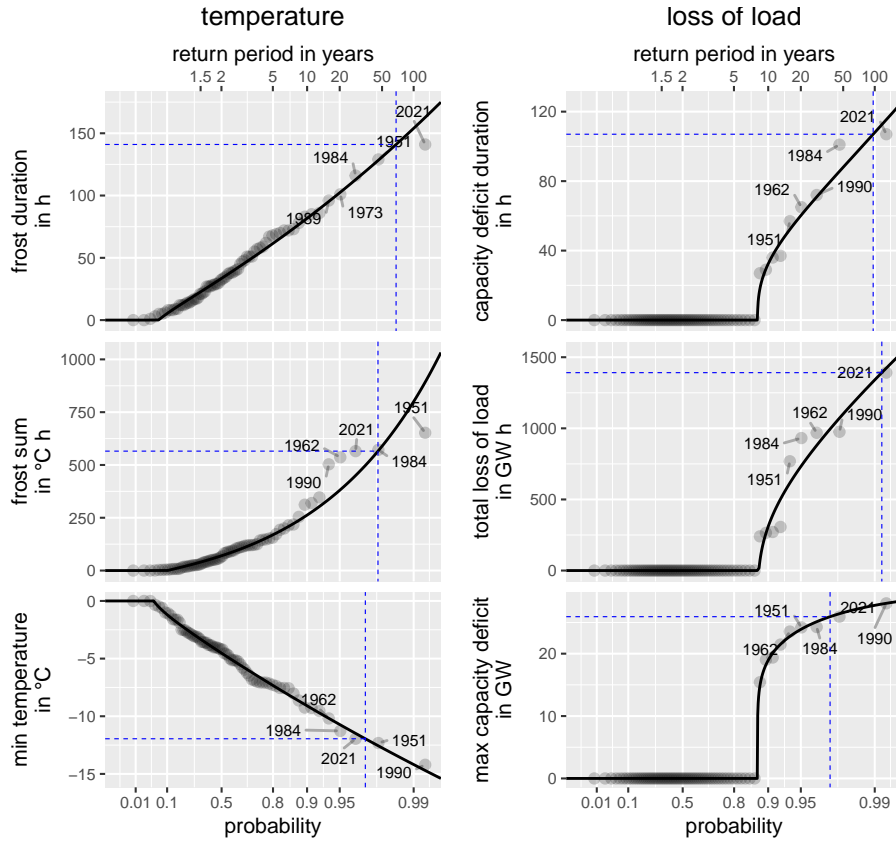


Figure A.3: Extreme value statistics of population weighted temperature (left panels) and predicted capacity deficit (right panels) of frost events in Texas from seven decades of climate data. Shown are the empirical (circles) and theoretical (lines) quantile functions of the three deficit characteristics, duration (upper), severity (centre) and intensity (lower). The return period (inferred from a GEV distribution) and magnitude of the 2021 event are annotated in blue

520 **A.3 Visualization of load prediction model**

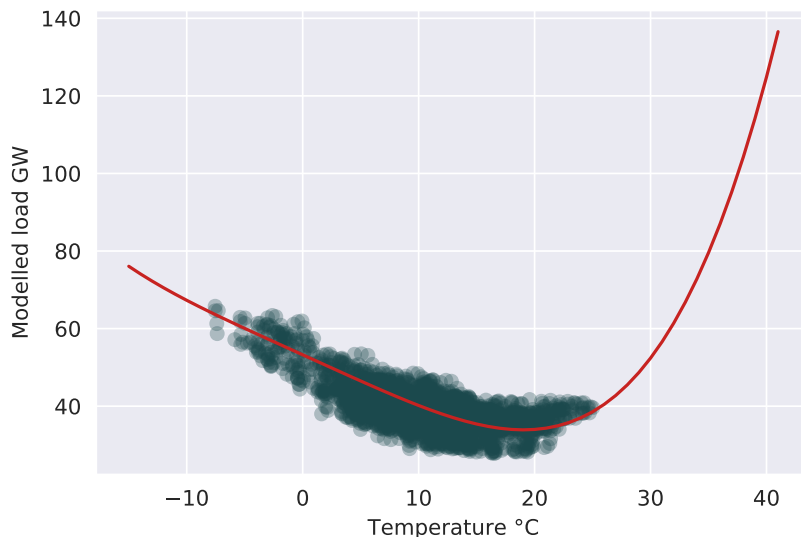


Figure A.4: Predicted load from 2018 data with constant time parameters for the range of Texas temperatures and load data for the winter period of 2018

521 **A.4 Approximation of outage functions**

522 We model the outages of the sum of capacities by technological group, defining an
523 outage model with 4 segments: (1) constant outage level before major critical failure,
524 (2) constant outage level during critical failure, (3) declining outage in recovery period,
525 and (4) constant outage level after recovery period (see Figures A.5 to A.8). (1) The
526 level of the first segment is defined by the first data point in the outage time series. The
527 first segment ends when the single largest increase in outage within one hour occurs
528 (i.e. the maximum of the first differences of the outage time series). The average power
529 plant capacity weighted temperature at that point is defined as outage temperature.
530 (2) The second segments starts at that point and ends when the temperature increases
531 above the recovery temperature, which is set to 0°C consistently for all technologies.
532 However, we neglect any hours with temperatures above the recovery temperature
533 within the first 10 hours after the start of the second segment. The level of the
534 plateau is derived by ensuring that the area below the real outage curve is the same
535 as the area below our modelled outage. (3) and (4) We extract the outage data from
536 the point of recovery to the end of the timeseries on the 25th of January. We then
537 fit a model to the data, which minimizes least squares. It contains two segments:
538 one falling recovery segment, and one constant segment at the end of the timeseries -
539 the level of that constant segment is defined as the average of the last ten points in
540 the time series. For segment (3), we can derive a slope after fitting, which is used as

541 parameter to simulate recovery. These models are applied to the whole 71 year long
 542 time series of temperature data, removing the constant outages at the beginning (1)
 543 and the end (4). An outage starts in the model, whenever the power plant capacity
 544 weighted temperature falls below the outage threshold. The full outage lasts until the
 545 temperature increases above the recovery temperature, but at least 10 hours. From
 546 that moment on, a linear, falling outage is assumed, until the outages is reduced to
 547 0GW.

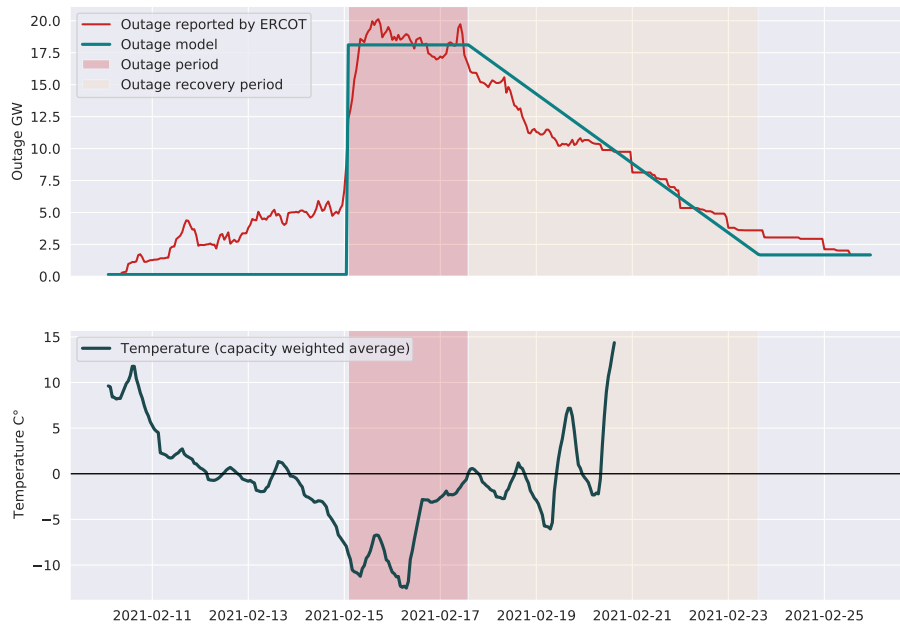


Figure A.5: Gas outages and temperature at gas power plants and approximated outage model

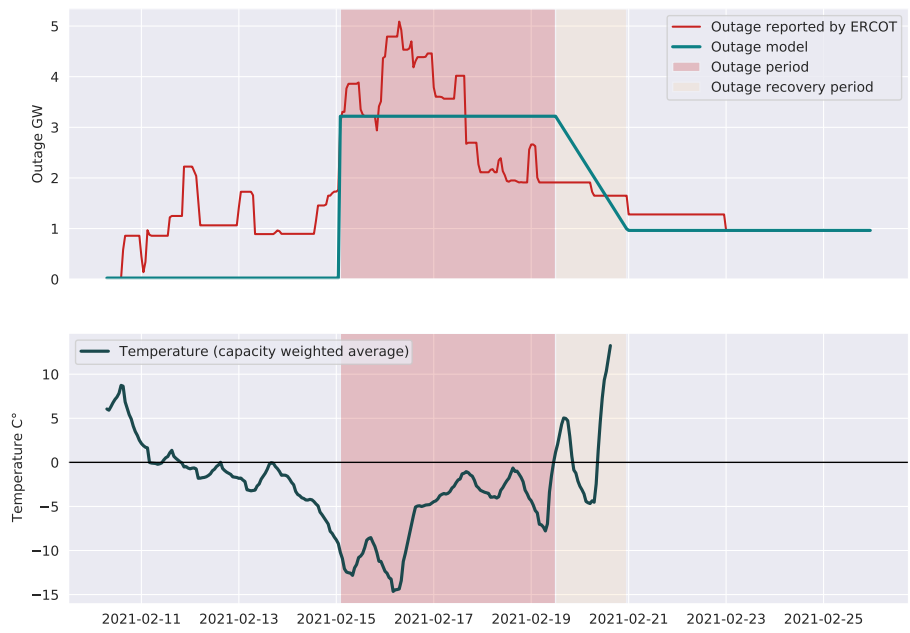


Figure A.6: Coal outages and temperature at coal power plants and approximated outage model

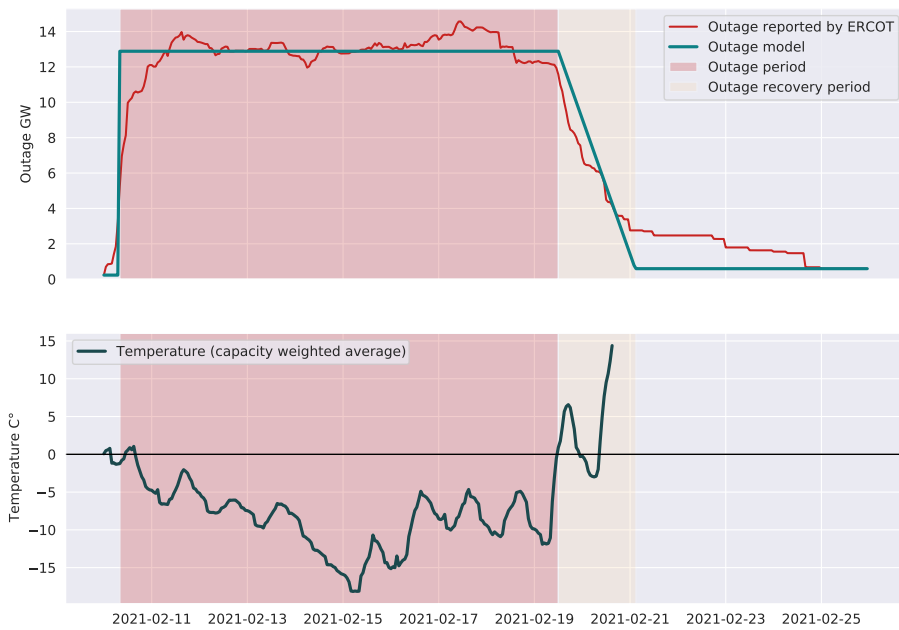


Figure A.7: Wind outages and temperature at wind power plants in Northern Texas and approximated outage model

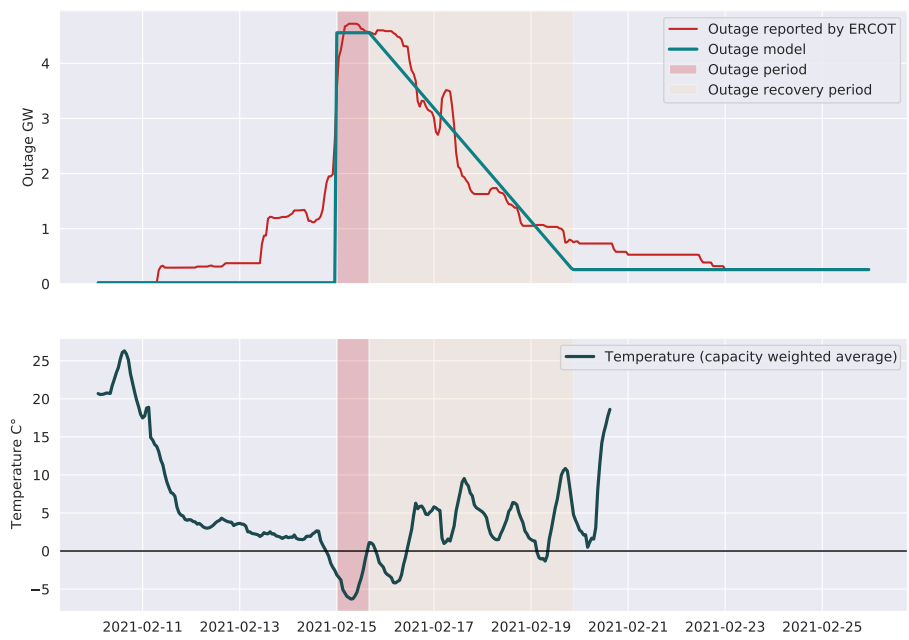


Figure A.8: Wind outages and temperature at wind power plants in Southern Texas and approximated outage model

548 **A.5 Trends in extreme events**

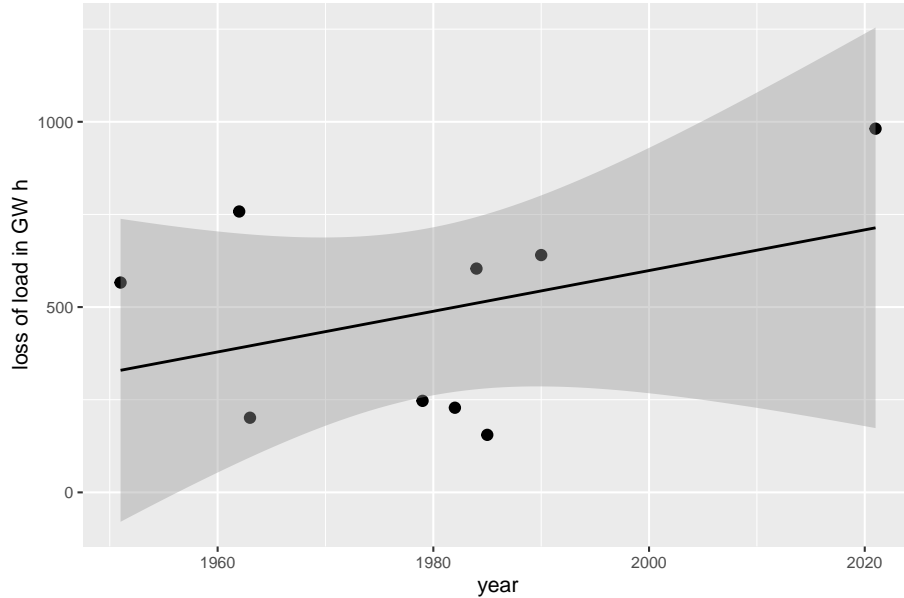


Figure A.9: Loss of load events in the period 1950–2021 with non-significant trend line (p-value=0.31)

549 **A.6 Modeling climate change trends in temperature**

550 Figure A.10 shows mean yearly population weighted temperatures over the past 71
 551 years. Regression indicates a clear trend towards higher average temperatures with an
 552 annual increase of 0.017°C.

553 In order to introduce an artificial linear trend to past temperatures, we increased all
 554 past temperatures by the trend observed in average temperature since 1950 assuming
 555 the linear trend of average temperatures would also translate to extreme tempera-
 556 tures, although there is no evidence of this phenomenon. Using the estimated average
 557 temperature trend of 0.017°C per year in the period 1950–2020, temperatures in the
 558 time series are updated in the following way:

$$t_{y,h}^{\text{trend}} = t_{y,h} + 0.017(y_{\text{ref}} - y) \quad (7)$$

559 We calculated two scenarios, using 2021 and 2050 as y_{ref} . These are the boundaries
 560 for our analysis, when considering a 30 years investment period.

561 **A.7 Trends in extreme temperature**

562 The predicted outage relies on the stationarity assumption for the temperature time
 563 series, in particular on the assumption that there is no trend in temperatures. We

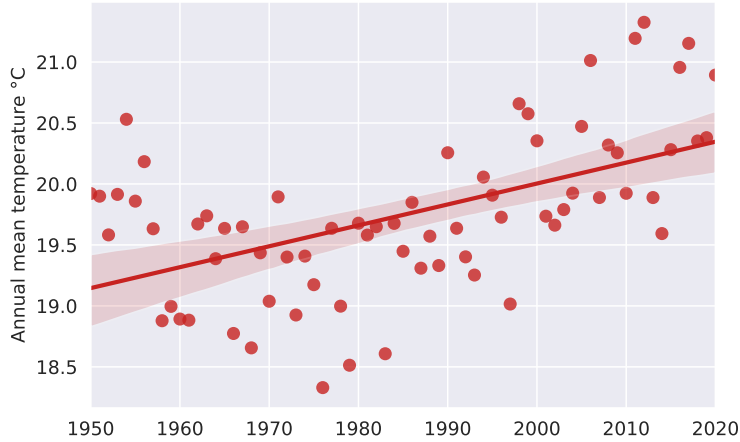


Figure A.10: Trends in population weighted annual mean temperatures

564 use past climate data to simulate outages. Due to climate change, we however ob-
 565 serve an increase in average temperatures in Texas. Our estimates may therefore be
 566 biased. Still, extreme events in the power system, in our model, occur at extremely
 567 low temperatures for the Texan context. These extreme cold events do not necessar-
 568 ily follow the trend in the average increase of temperatures [12]. Our model uses a
 569 minimum threshold of $-10.2\text{ }^{\circ}\text{C}$ for coal, $-8.8\text{ }^{\circ}\text{C}$ for gas, -10.9 for gasfields, $-1.2\text{ }^{\circ}\text{C}$ for
 570 wind in Northern Texas and $-3.1\text{ }^{\circ}\text{C}$ for wind outages in Southern Texas. Therefore,
 571 we specifically need to examine stationarity of annual minimum temperatures below
 572 this threshold. By conducting a robust trend analysis for annual temperature minima
 573 below the threshold for different temperature thresholds, we find that extreme frost
 574 events in Texas only show a trend if the temperature threshold is set to $-1\text{ }^{\circ}\text{C}$ or above,
 575 i.e. very high. For temperature thresholds below $-1\text{ }^{\circ}\text{C}$, no trend can be confirmed (see
 576 Table A.1). Assuming a trend in a reduction of extreme cold events below $-1\text{ }^{\circ}\text{C}$ can
 577 therefore not be confirmed by the 71 years of temperature data available to us.
 578

579 A.8 Calculation of winterization costs

580 There is very limited information on winterization costs available from media reports.
 581 For gas wells, costs of 50,000\$ for winterization are reported [27]. Winterizing all
 582 123,000 gas wells in Texas [29] would therefore yield a total cost of 6.15bn\$. 18GW of
 583 gas power capacity failed during the 2021 event according to our simulation. Conser-
 584 vatively assuming that winterization costs of gas fields can be split according to failed
 585 gas power capacity, winterization costs for gas fields of 342 Mio\$/GW of gas power
 586 plant capacity can be derived. This is equivalent to around 250GWh of pipe storage
 587 for methane, which could be installed on the site of gas power plants to secure supply
 588 under cold conditions as alternative [30]. Assuming costs of gas power plant winteri-
 589 zation to be 10% of investment costs, total winterization costs result in 453 Mio\$/GW
 590 of gas power capacity at an investment costs for gas power plants of 1.12bn\$/GW [31].

Table A.1: Trends in cold temperature with different temperature thresholds

temperature threshold	events	slope yearly	slope 71 years	p-value
0	71	0.037	2.65	0.029
-1	70	0.037	2.61	0.033
-2	63	0.020	1.43	0.256
-3	55	0.004	0.30	0.816
-4	38	-0.005	-0.38	0.810
-5	30	-0.002	-0.11	0.948
-6	25	0.013	0.95	0.547
-7	20	0.018	1.27	0.474
-8	10	-0.028	-1.96	0.316
-9	8	-0.017	-1.22	0.422
-10	5	-0.013	-0.89	0.491

591 For coal and wind power plants, no infrastructure has to be winterized. Therefore, win-
592 terization costs will be significantly lower than for gas. Winterization of wind turbines
593 is about 5% [14] of investment costs. Assuming investment costs of to 1.3bn\$/GW
594 [32], this yields 65 Mio\$/GW of wind power capacity as estimate of winterization costs
595 for wind turbines.

596 For coal power plants, we did not find any estimate, and assume 10% of investment
597 costs. At investment costs for coal power plants of 2.24 bn\$/GW [31], winterization
598 costs of 224 Mio\$/GW are obtained.