

# Sorting lithium-ion battery electrode materials using dielectrophoresis

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## Abstract

Lithium-ion batteries (LIBs) are common in everyday life and the demand for their raw materials is increasing. Additionally, spent LIBs should be recycled for achieving a circular economy and supply resources for new LIBs or other products. Especially the recycling of the active material of the electrodes is in the focus of current research. Existing approaches for the recycling (e.g., pyro-, hydrometallurgy or flotation) still have their drawbacks, such as the loss of material, generation of waste, or lack of selectivity. In this study, we test the behavior of commercially available LiFePO<sub>4</sub> and two types of graphite microparticles in a dielectrophoretic high-throughput filter. Dielectrophoresis is a volume dependent electrokinetic force that is commonly used in

11 microfluidics but recently also for applications that focus on enhanced throughput. In  
12 our study, graphite particles show significantly higher trapping than  $\text{LiFePO}_4$  particles.  
13 The results indicate that nearly pure fractions of  $\text{LiFePO}_4$  can be obtained with this  
14 technique from a mixture with graphite.

## 15 **1 Introduction**

16 Lithium-ion batteries (LIBs) power electrical devices in nearly all parts of modern society.  
17 For example, LIBs are used in portable electronics and electric vehicles. Consequently, the  
18 demand for LIB resources grows.<sup>1</sup> To recover materials of spent LIBs, the recycling of elec-  
19 trodes is a focus of current research. As about one half of the weight of LIBs consists of  
20 the active material of anode and cathode, their recycling is desirable.<sup>2</sup> Cathode active ma-  
21 terials typically are lithium metal oxides (e.g.,  $\text{LiCoO}_2$ ,  $\text{LiFePO}_4$  or  $\text{LiNi}_{1/3}\text{Mn}_{1/3}\text{Co}_{1/3}\text{O}_2$ ),  
22 whereas graphite is common for anodes.<sup>1,2</sup> Anode and cathode consist, among carbon black  
23 as conductive additive and a polymer binder, of a current collector (Cu or Al foil) to which  
24 the active material adheres.<sup>2-4</sup> Current collector and active material can be separated by  
25 both, chemical and mechanical approaches, such as crushing and sieving.<sup>1,3-5</sup> Typically, one  
26 product of these processes is the so-called black mass, a mixture from anode and cathode  
27 active material.<sup>4</sup> Current recycling techniques for black mass are, for example, pyro- or hy-  
28 drometallurgical and focus on the recovery of cathode active material because of its higher  
29 value compared to graphite. Graphite might be lost or burned as energy source within the  
30 recycling process.<sup>1,2,5-7</sup> Yet processes exist where graphite can be recovered. In hydrometal-  
31 lurgical approaches, the lithium metal oxides are dissolved in acid during a leaching step and  
32 recovered in subsequent unit operations. Graphite can simply be recovered by filtration after  
33 the leaching step.<sup>4</sup> But as significant amounts of liquid wastes are produced in this recycling  
34 pathway<sup>8</sup> it would benefit from an efficient sorting step before the leaching to reduce the  
35 amount of chemicals needed. As the active materials are essentially microparticles,<sup>9-11</sup> di-  
36 rect recycling using particle separation techniques could play a vital role within the recycling

37 process to enhance or replace existing recycling approaches of LIBs. One approach which is  
38 well established for particulate systems and capable of handling large amounts of product  
39 is flotation, which was also applied to separate black mass. This works because anode and  
40 cathode material show different wettability.<sup>5,7,12-14</sup> However, according to Neumann et al.,<sup>4</sup>  
41 the process needs to be optimized further as the achievable recovery rates are currently too  
42 low. Other direct approaches that utilize, for example, eutectic salts or ionic liquids can be  
43 found in two recent reviews<sup>15,16</sup> that elaborate these techniques in more detail than it is the  
44 scope of this study.

45 This paper investigates the possibility to address particles found within black mass using  
46 dielectrophoresis (DEP) at high throughput. DEP is the movement of a polarizable particle  
47 in an inhomogeneous electric field. Usually, it is used in the biomedical field and primarily in  
48 microfluidic devices.<sup>17,18</sup> Although DEP is label-free, has high selectivity, and the capability  
49 of addressing nano- to micrometer-scaled particles,<sup>19-21</sup> few studies addressed recycling or the  
50 throughput that would be required for this.<sup>22-27</sup> While DEP is well studied with biological  
51 samples, such as DNA<sup>28,29</sup> and cells,<sup>30-33</sup> the separation of non-biological particles, aside  
52 from polystyrene particles, is rarely described in literature.<sup>18</sup> This study is designed to  
53 expand this field by using artificial black mass to show that conductive particles can be  
54 addressed with an electrode-based DEP separator at high throughput. By using a setup  
55 based on printed circuit boards (PCBs), we assess the behavior of  $\text{LiFePO}_4$  and graphite  
56 microparticles and their mixture under the influence of DEP. To the best of the authors'  
57 knowledge the separation of LIB electrode material using dielectrophoresis has not yet been  
58 addressed. This study aims to serve as a starting point for future research in this field  
59 by describing the possibilities and limitations of DEP as a separation technique for these  
60 materials.

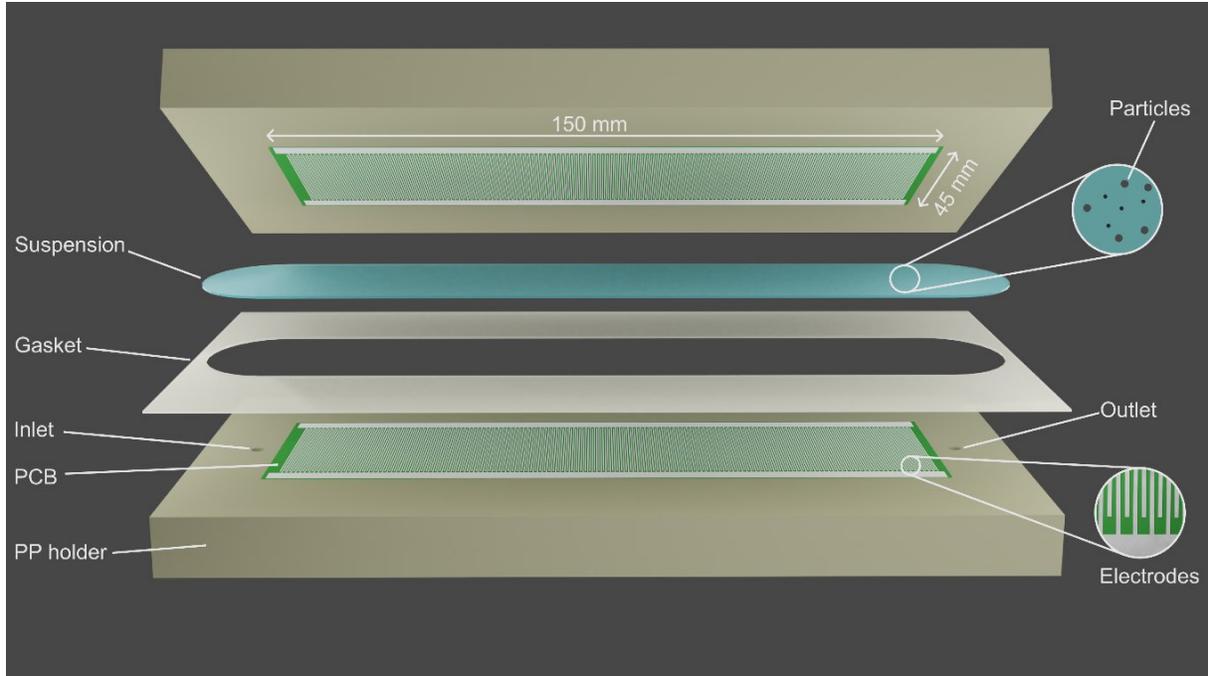


Figure 1: Rendered overview of the separator. The suspension is pumped from inlet to outlet through a channel formed by two printed circuit boards (PCBs), a silicon gasket and the polypropylene (PP) holders. The PCBs feature an interdigitated electrode structure (bottom right insert) that are used to generate a highly inhomogeneous electric field.

## 2 Materials and Methods

### 2.1 Dielectrophoretic separator

The separator used in this study is an updated version of the one which was evaluated and published in Ref. 25 and is designed to selectively trap particles when an electric field is applied. An overview of the device can be seen in Figure 1. The key feature of this device are two inexpensive ( $< 1\text{€}/\text{pc.}$ ) custom designed PCBs (manufactured by JiaLiChuang (HongKong) Co., Limited, China) with a size of  $45 \times 150$  mm, which is slightly different from the previous design.<sup>25</sup> The improved design showed similar performance with reduced PCB size and energy demand. The new design has an impedance of  $20 \Omega$  at 500 kHz in comparison to  $13 \Omega$  from the old design. The PCBs are covered by an interdigitated electrode array with an electrode width and spacing both being  $250 \mu\text{m}$ . The two PCBs face each other and are separated by a 0.5 mm silicone gasket. The two PCBs together

73 with the gasket form a channel. The gasket is manually cut to form a channel that is  
 74 about 175 mm  $\times$  38 mm  $\times$  0.5 mm (L $\times$ W $\times$ H) and thus has a theoretical volume of 3.33  
 75 mL. We additionally measured the volume using a scale and found that the actual volume is  
 76 2.8 mL $\pm$ 0.1 mL, which is slightly lower and likely caused by a compression of the sealing. The  
 77 calculated height of the sealing results to be 0.42 mm. This gives a average residence time  
 78 of 28 s at 6 mL/min and 17 s at 10 mL/min in the channel. Consequently, at 6 mL/min,  
 79 an average velocity of 6.3 mm/s can be expected and of 10.4 mm/s at 10 mL/min. The  
 80 electrodes are connected to a power amplifier (F30PV, Pendulum Instruments, Sweden)  
 81 which is capable of providing up to 75 V<sub>pp</sub> at maximum current of 2 A. The sinusoidal  
 82 signal was generated by a signal generator (Rigol DG4062, Rigol Technologies EU GmbH,  
 83 Germany), monitored using an oscilloscope (Rigol DS2072A, Rigol Technologies EU GmbH,  
 84 Germany) and power analyzer (PPA1510, Newtons4th Ltd, Leicester, United Kingdom).  
 85 The suspension was pumped using a piston pump (Ismatec MCP-CPF IP65 with pump  
 86 head FMI 202 QP.Q0.SSY, Cole-Parmer GmbH, Germany).

87 The operating principle is described in detail elsewhere.<sup>25</sup> Briefly, DEP can be an at-  
 88 tractive force (positive DEP/pDEP) if a particle is better polarizable than the surrounding  
 89 medium or a repulsive force (negative DEP/nDEP) when the particle is less polarizable. Pos-  
 90 itive DEP guides particle towards local field maxima, whereas nDEP pushes particles away  
 91 from them.<sup>17</sup> This can lead to a separation as was previously shown several times.<sup>25,34,35</sup>  
 92 Whether a particle experiences pDEP or nDEP depends on the real-part of the Clausius-  
 93 Mossotti factor ( $CM$ ), which is defined as<sup>17</sup>

$$\text{Re}(CM) = \text{Re} \left( \frac{\tilde{\epsilon}_p - \tilde{\epsilon}_m}{\tilde{\epsilon}_p + 2\tilde{\epsilon}_m} \right), \quad (1)$$

94 with the complex permittivity  $\tilde{\epsilon} = \epsilon_0 \epsilon_r - i \frac{\sigma}{\omega}$ . The complex permittivity incorporates not only  
 95 the permittivity  $\epsilon$  but also the angular frequency of the electric field  $\omega$  and the conductivity  
 96 of a material  $\sigma$ .  $\text{Re}(CM)$  is bound between  $-0.5$  and  $1.0$  and is negative in case of nDEP

97 and positive in case of pDEP. Finally, the DEP force  $\mathbf{F}_{\text{DEP}}$  for a spherical and homogeneous  
 98 particle can be approximated as

$$\mathbf{F}_{\text{DEP}} = 2\pi r_p^3 \varepsilon_m \text{Re}(CM) \nabla |\mathbf{E}_{\text{rms}}|^2 \quad (2)$$

99 with  $r_p$ , the radius of the particle, the electric field,  $\mathbf{E}_{\text{rms}}$ , and the permittivity of the sur-  
 100 rounding medium,  $\varepsilon_m$ . Conductive particles in a medium with low conductivity, as used  
 101 in this study, will usually experience pDEP.  $\mathbf{F}_{\text{DEP}}$  is not only depending on the particle  
 102 and medium polarizability but also on the particle volume ( $r_p^3$ ) which is important in the  
 103 following.

## 104 2.2 Particles

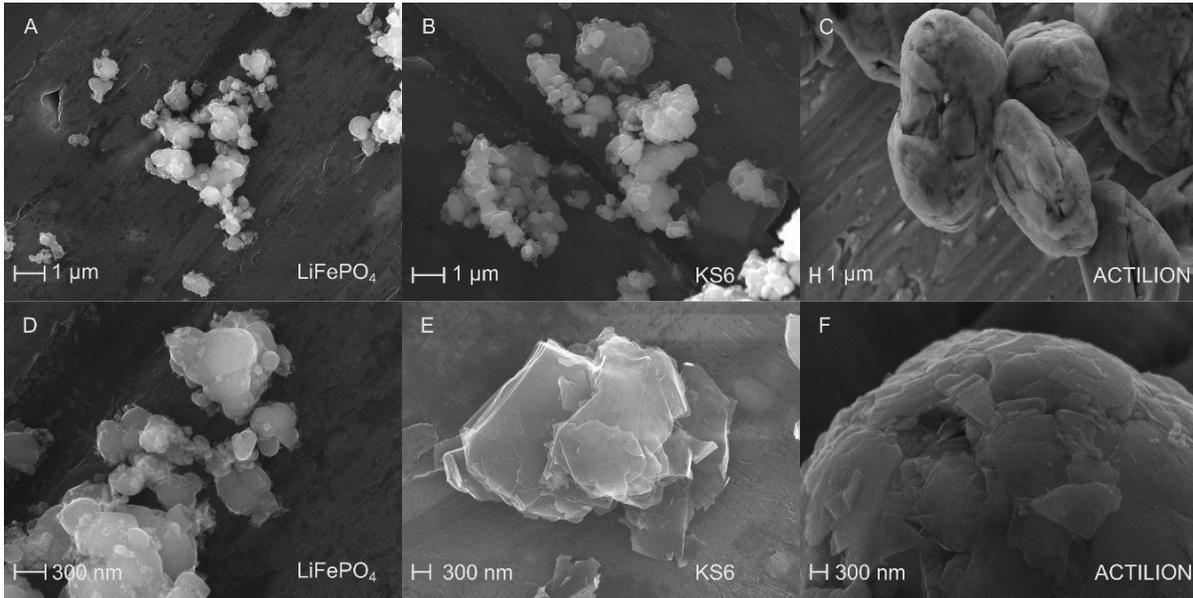


Figure 2: SEM images of  $\text{LiFePO}_4$  (A&D), KS6 synthetic graphite (B&E) and C-ENERGY Actilion GHDR 15-4 (C&F) microparticles. The scale bar in the top row equals  $1 \mu\text{m}$  and  $300 \text{ nm}$  in the bottom row. Please note that the magnification and consequently the scale bar varies in size.

105 The particles investigated here all are commercially available and are specifically designed  
 106 for battery research. We chose  $\text{LiFePO}_4$  (Nanografi Nano Teknoloji AS, Turkey) as a cathode

107 material, not only because it is widely used for LIBs but also because it is considered to  
108 have low toxicity, which makes it more convenient to work with.<sup>11,36,37</sup> LiFePO<sub>4</sub> as cathode  
109 material is carbon coated to enhance its otherwise poor conductivity (about 10 nS/cm<sup>-1</sup>).<sup>38,39</sup>  
110 This leads, according to the distributor, to an electrical conductivity of 0.88 S/m. The used  
111 LiFePO<sub>4</sub> shows a distributed particle size from several hundred nm to a few  $\mu\text{m}$  (Table 1,  
112 Figure 2 A&D). The small size of the LiFePO<sub>4</sub> particles and its high specific surface area  
113 is a result from design optimization as this is favorable for the performance of batteries.<sup>40</sup>  
114 This is in the range of sizes mentioned in the literature for application on LIB<sup>41-44</sup> and also  
115 in the range of the size reported for some other cathode materials.<sup>45</sup> Additionally, two types  
116 of graphite particles were selected. Timrex KS6 (MSE Supplies LLC, USA) is a synthetic  
117 graphite with high purity which can be used as conductive additive for anodes and cathodes.  
118 According to the manufacturer (Imerys Graphite & Carbon, Switzerland), it is larger than  
119 the LiFePO<sub>4</sub> particles (Table 1, Figure 2 B&E). The second type of graphite C-ENERGY  
120 Actilion GHDR 15-4 (provided by Imerys Graphite & Carbon, Switzerland), here referred to  
121 as Actilion, is an active material for anodes of LIBs and significantly larger than the other  
122 two materials (Table 1, Figure 2 C&F). The larger size of graphite that is used as active  
123 material in anodes in LIBs was also described in the literature<sup>10,11,44</sup> and again is a results  
124 from optimizing the battery performance<sup>46</sup>. Both graphite and LFP are highly conductive  
125 compared to the suspension and thus will show pDEP at all frequencies used in this study  
126 (see supporting information S6). Therefore, all particles will move towards field maxima  
127 which are located at the edges of the electrode array on the PCBs. As the sizes of the  
128 particles here diverge significantly, we aim to exploit the linear volume dependence of  $\mathbf{F}_{\text{DEP}}$   
129 to achieve a separation.

130 The size differences of graphite and LiFePO<sub>4</sub> particles are critical for a size dependent  
131 sorting as it is conducted in this study. This difference may be affected by an upstream  
132 liberation step that produces black mass. This, however, depends strongly on the liberation  
133 step itself. Mu et al.<sup>47</sup> described for cathode material, here LiCoO<sub>2</sub>, no apparent size changes

134 when liberating the particles with calcination or supercritical CO<sub>2</sub>. The liberation of particles  
 135 from black mass during the recycling of spent LIBs is a separate field of research and not  
 136 part of this study. Artificial black mass is used here to exclude effects upstream processes,  
 137 focus on separability under ideal conditions and facilitate reproducibility.

Table 1: Parameters describing the size distribution of the used particles

Particle	d <sub>10</sub> / μm	d <sub>50</sub> / μm	d <sub>90</sub> / μm
LiFePO <sub>4</sub>	0.6	1.5	6.0
KS6	1.5	3.4	6.1
Actilion	13	17	23

### 138 2.3 Measurement system

139 Two methods were used to measure the particle separation. Qualitatively, the total particle  
 140 concentration was measured by white-light reflection in real-time at the outlet. Quanti-  
 141 tatively, the LiFePO<sub>4</sub> concentration was further evaluated using photometric detection of  
 142 dissolved iron mass. The reflection measurement system is described in Ref. 25. Briefly, it  
 143 consists of a spectrometer (Silver nova, StellarNet, Inc., USA) and a flow cuvette (176-765-  
 144 85-40 and 176-760-85-40, Hellma GmbH & Co. KG, Germany). A white light source (XCite  
 145 120 PC, Excelitas Technologies Corp., USA) is connected in 90° with respect to the light  
 146 guide of the spectrometer. Particles in the flow cuvette will scatter the light and produce  
 147 a signal that can be recorded by the spectrometer. For size-distributed particle systems,  
 148 it is important to keep in mind that the reflection intensity varies with particle size. For  
 149 spheres in the size range of the particles used here and the wavelength of the light source,  
 150 the scattering intensity is proportional to  $r_p^2$ .<sup>48</sup> As the particles here are not perfect spheres  
 151 (Figure 2), the signal recorded by the spectrometer does not provide the information of the  
 152 number or mass of eluted particles, which is different compared to monodisperse particulate  
 153 systems as in Ref. 25 and 22. This certainly is a downside of the reflection measurement  
 154 setup. We thus use the measured reflective light intensity reduction at the outlet as a qual-  
 155 itative real-time indicator of particle retention. To measure the retention of LiFePO<sub>4</sub> in the

156 filter, we used a chemical procedure which allows a photometric determination of the iron  
157 mass. The procedure was derived from DIN 38406 (see supporting information S5). Briefly,  
158 the  $\text{LiFePO}_4$  particles are dissolved in an acid and the iron content is determined using a  
159 complexing agent and performing a photometric measurement afterward.<sup>49</sup>

## 160 **2.4 Experimental procedure**

161 Experiments were carried out in a low-conductivity medium ( $2.1 \mu\text{S}/\text{cm}$ ) consisting of pure  
162 water (Omniatap 6 UV/UF, stakpure GmbH, Germany), 0.01 vol.% Tween 20 (Sigma–Aldrich,  
163 Germany), and KCl to adjust the conductivity. A low conductivity medium was selected as  
164 this reduces the influence of thermal effects. For future applications, the impact of an in-  
165 creased conductivity needs to be investigated as this may have an impact on the separation.  
166 The black mass used in this study is artificial. Consequently, the impact of residuals from an  
167 upstream process that produces actual black mass is not considered and beyond the scope of  
168 this study. To create particle stock suspensions, the particles were suspended in an 1 vol.%  
169 aqueous Tween 20 suspension with 4 g/L for  $\text{LiFePO}_4$  and KS6 and 12 g/L for Actilion. The  
170  $\text{LiFePO}_4$  suspension was renewed every three days as Li is known to dissolve to a low extend  
171 into aqueous solutions,<sup>50</sup> and we wanted to exclude this effect from our experiments. Prior  
172 to the experiments, we sonicated the particle stock suspensions and added 0.22 vol.% of it,  
173 for  $\text{LiFePO}_4$  and KS6, into the medium for the experiments. In order to achieve a sufficient  
174 reflection signal, we had to increase the Actilion concentration, resulting in a  $10\times$  higher  
175 total mass of Actilion in the final suspension compared to the other two particle types. The  
176 reason behind this might be lower specific surface area of the larger Actilion particles and  
177 thus lower reflectance per added mass.

178 The suspensions were stirred throughout the entire experiment. To subtract the back-  
179 ground signal, we recorded the intensity signal daily with no particles present (supporting  
180 information S2). At the beginning of the experiments we measured the initial reflection  
181 signal of the particle suspension for 30 s. At 30 s the electric field was turned on for 270 s.

182 After the voltage was turned off, the experiment was further monitored until the initial in-  
183 tensity was obtained again. Sometimes, the initial signal was not fully reached due to effects  
184 such as sedimentation or bubble adhesion in the flow-through cuvette. As a consequence we  
185 flushed the entire setup at a high flow rate after every two experiments. Every data point  
186 represents three experiments. Equation 1 in section S1 of the supplement details how the  
187 signal reduction is calculated.

188 To chemically determine the retention of the  $\text{LiFePO}_4$  particles, we collected 4 mL of  
189 suspension in a 5 mL container. The samples were taken at the beginning of the experiment,  
190 starting after 5 s and during the trapping, starting after 200 s. In order to obtain a sufficient  
191 sample volume at the beginning of the experiment, the voltage was turned on after 60 s.

192 All data from the reflection measurements, the evaluation script (MATLAB, details see  
193 supporting information S1) and PCB manufacturing data are uploaded to an online reposi-  
194 tory (Ref. 51).

## 195 **3 Results and Discussion**

### 196 **3.1 Frequency dependent behavior up to 500 kHz**

197 All particles in this study are conductive and thus should show pDEP. To test this hypothesis,  
198 we conducted experiments at 30 V<sub>pp</sub> from 1 kHz to 500 kHz at a volume flow of 6 mLmin<sup>-1</sup>  
199 with only one particle type present per experiment (Figure 3). Higher frequencies were  
200 not applicable in this setup and the selected voltage, because the required current would  
201 exceed the maximum of the amplifier. For all particles the trapping efficiency (measured  
202 qualitatively in terms of reduction of reflective light intensity signal, called signal reduction)  
203 was highest at 500 kHz and significantly higher than at lower frequencies. This might be  
204 because disturbing electrokinetic effects like AC electroosmosis can be dominant at lower  
205 frequencies.<sup>52</sup> However, as the frequency significantly exceeds the electrothermal hydrody-  
206 namic relaxation frequency ( $f = \sigma_m / (2\pi\epsilon_m) \approx 48$  kHz), this effect should be negligible.<sup>53</sup>

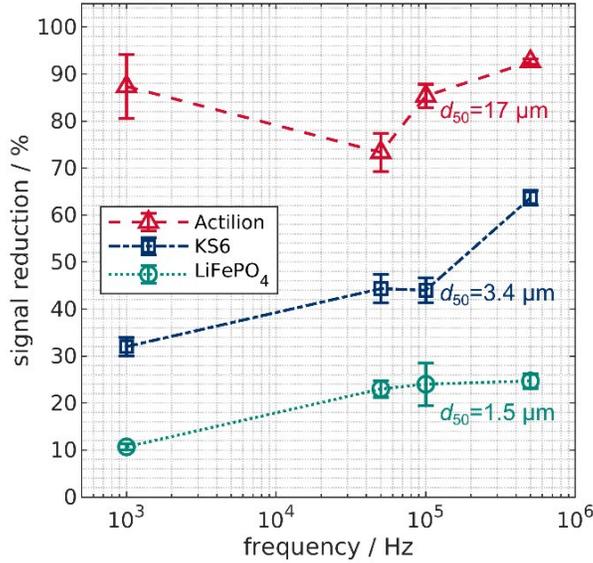


Figure 3: Frequency dependency of the signal reduction of Actilion, KS6 and LiFePO<sub>4</sub> suspensions at 6 mLmin<sup>-1</sup> and 30 V<sub>pp</sub>. Frequencies were varied between 1 kHz and 500 kHz.

207 Currently, we are not sure what is causing the reproducible further trapping increase and  
 208 thus signal reduction with an additional increase in frequency. Nonetheless, significant dif-  
 209 ference in the signal reduction becomes apparent when comparing the particle types. This is  
 210 likely caused by the differences in particles size as DEP scales with particle volume (Equation  
 211 2). For example, at 30 V<sub>pp</sub> and 500 kHz, Actilion shows a high signal reduction of  $93 \pm 0.6$  %  
 212 but the signal of LiFePO<sub>4</sub> is only reduced by  $26 \pm 1.5$  %. To further investigate the be-  
 213 havior of the particles, we selected 500 kHz as frequency for all subsequent experiments,  
 214 because the performance of the device is the highest at this frequency and DEP the domi-  
 215 nating force. We note that a direct quantitative comparison between the different particles  
 216 types may be misleading. This is because the scatter properties between distributed parti-  
 217 cle samples may be different due to different shapes. The qualitative comparison, however,  
 218 reveals significant differences that agree well with the proposed size selectivity. The appli-  
 219 cation of 500 kHz also demonstrates that frequencies in this range can be applied in a high  
 220 throughput device. Compared to previous high-throughput approaches by our group<sup>22-24</sup>  
 221 that were insulator-based DEP devices, the applicable frequency bandwidth was expanded

222 from 75 kHz to 500 kHz while maintaining the possibility of applying high volume flows. A  
223 higher possible frequency can be beneficial when designing the process as with increasing  
224 frequency the polarizability can alter and enable a separation. In a previous study we could  
225 show that retention due to nDEP is small ( $< 10\%$ ) in such a setup and therefore is not the  
226 reason for our observations.<sup>25</sup>

### 227 **3.2 Influence of voltage and volume flow**

228 As second step, we investigated the influence voltage on signal reduction from 5 to 75  $V_{pp}$   
229 at 6  $\text{mLmin}^{-1}$  (Figure 4A) and 10  $\text{mLmin}^{-1}$  (Figure 4B). At both flow rates, all particles  
230 show an increased signal reduction or particle retention with increasing voltage. This is in  
231 line with the approximation of the DEP force (Equation 2). Additionally, increasing volume  
232 flow decreases the signal reduction. This is due to the increased viscous drag and decreased  
233 residence time in the setup at the higher flow rate. The data at 6  $\text{mLmin}^{-1}$  and 30  $V_{pp}$   
234 is the same as in Figure 3, except for Actilion. Here, we used a different flow cuvette for  
235 this measurements to prevent sedimentation. However, the results are quite similar (here  
236  $97 \pm 2.7\%$  compared to  $93 \pm 0.6\%$ ). Figure 4 C-E shows intensity plots over time for all  
237 particles at 30  $V_{pp}$  and 10  $\text{mLmin}^{-1}$ . Three things become apparent from Figure 4. First,  
238 the signal reduction of Actilion is significantly higher than that of  $\text{LiFePO}_4$ . For example, at  
239 30  $V_{pp}$  and 10  $\text{mLmin}^{-1}$  (Figure 4 B,C and E), the signal reduction of Actilion is over four  
240 times higher than it is for  $\text{LiFePO}_4$ . Here, the recorded intensity for Actilion is close to zero,  
241 indicating a complete removal. The relative difference of the signal reduction of  $\text{LiFePO}_4$   
242 and Actilion, however, decreases with increasing voltage (Figure 4A and B). Likely, this is  
243 because Actilion is already almost completely removed at voltages over 30  $V_{pp}$  at both flow  
244 rates, whereas  $\text{LiFePO}_4$  removal increases with voltage from 0 to 75  $V_{pp}$ . Second, KS6 also  
245 shows significant trapping and gets fully removed at about 75  $V_{pp}$  at both flow rates. Third,  
246 the reflection measurements can create signal reduction slightly higher than 100 % which is  
247 linked to the subtraction of the background signal and was observed before.<sup>25</sup> The highest

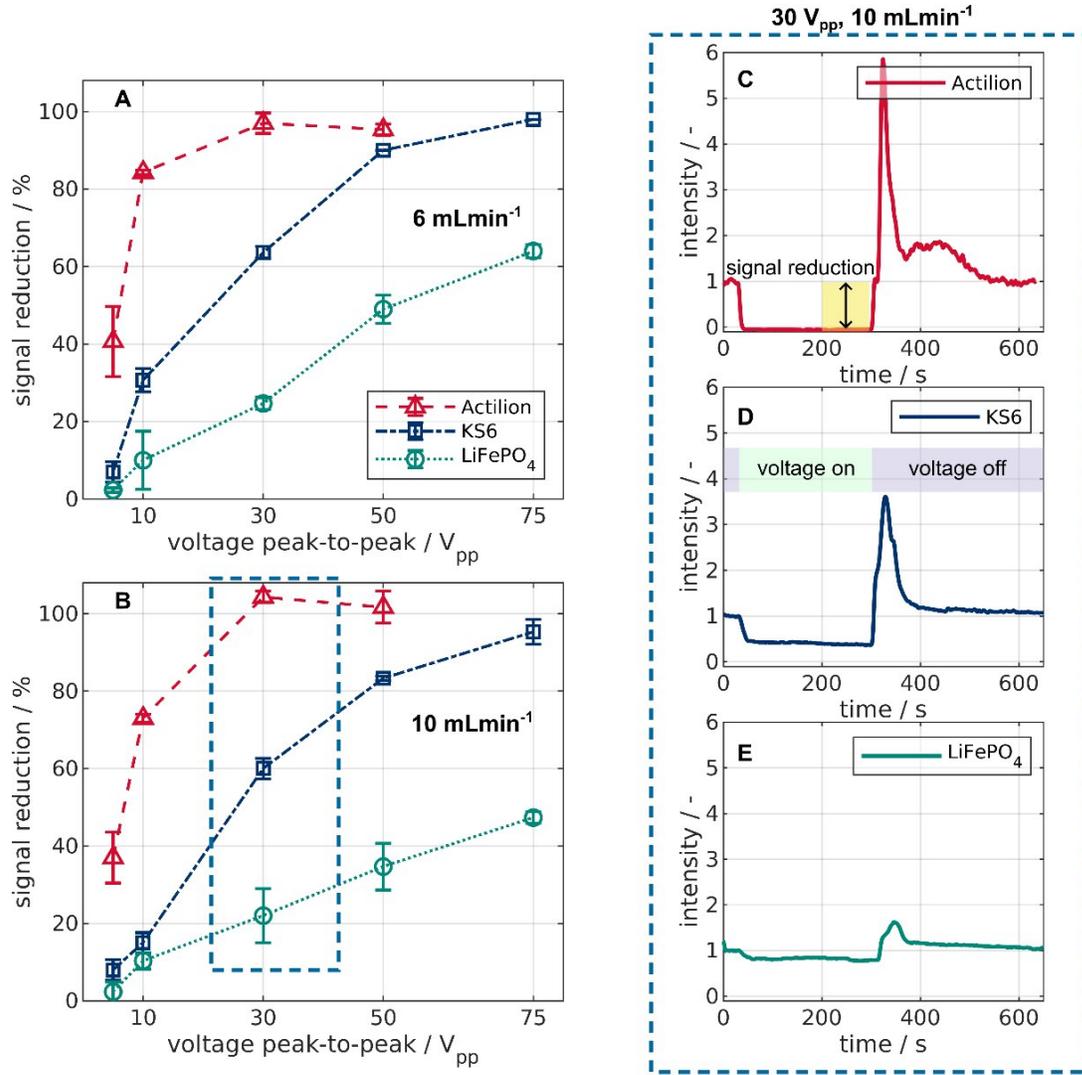


Figure 4: Voltage and volume flow dependency of the signal reduction for Actilion, KS6 and LiFePO<sub>4</sub> suspensions at a frequency of 500 kHz. The behavior was evaluated between 5 and 75 V<sub>pp</sub> at 6 mLmin<sup>-1</sup> (A) and 10 mLmin<sup>-1</sup> (B). As example, normalized reflection intensities over time for all materials at 30 V<sub>pp</sub> and 10 mLmin<sup>-1</sup> are also shown (C-E). For all experiments, the signal reduction was measured between 200 and 300 s (C). The voltage was applied after 30 s for 270 s (D).

248 recorded value was  $104 \pm 1.5\%$  at  $10 \text{ mLmin}^{-1}$  and  $30 V_{pp}$ . As the deviation is explainable  
 249 (supporting information S2), relatively small, and showing a complete removal of Actilion,  
 250 we do not consider this problematic.

251 In summary, the size, voltage, and volume flow dependency of the signal reduction for  
 252 these particles was as expected. In addition, we observed an almost complete removal of  
 253 Actilion from the suspension starting at  $30 V_{pp}$ . For mixtures of  $\text{LiFePO}_4$  and Actilion,  
 254 this would correspond to a pure fraction of  $\text{LiFePO}_4$  at the outlet and an enrichment of  
 255 Actilion within the filter. Higher voltages than  $30 V_{pp}$  would not lead to a significantly  
 256 increased trapping of Actilion but to more retained  $\text{LiFePO}_4$ . Therefore, we selected  $30 V_{pp}$   
 for separation experiments of Actilion and  $\text{LiFePO}_4$ .

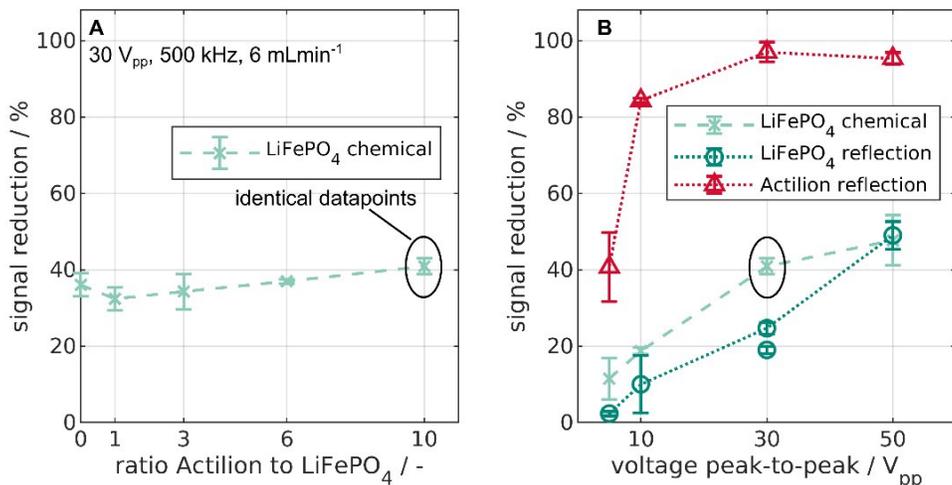


Figure 5: A: Variation of the mass ratio of  $\text{LiFePO}_4$  and Actilion graphite particles in the suspension at  $30 V_{pp}$ ,  $500 \text{ kHz}$  and  $6 \text{ mLmin}^{-1}$ . B: Comparison of reflection measurements of suspensions with only one particle type present (dotted lines) and the chemical analysis of  $\text{LiFePO}_4$  removal from a mixture with 10 times more mass of Actilion than  $\text{LiFePO}_4$  (dashed line).

257

### 258 3.3 Behavior in a mixture of graphite and $\text{LiFePO}_4$

259 As a final step, we investigated the separability of a mixture of  $\text{LiFePO}_4$  and Actilion.

260 We did not include KS6 because conductive additives are only around 4 % of the battery

261 mass.<sup>2</sup> It would further increase the difficulty of analyzing the results because the reflection  
262 measurement is not material sensitive. We tried to calculate separate reflection spectra for  
263 each component by superposition of the reflection spectra of pure  $\text{LiFePO}_4$  and Actilion,  
264 as they are slightly different. For fluorescent particles this can be achieved by coupling  
265 these reference spectra with a global optimization to calculate separate intensities over time  
266 distributions as described in Ref. 24. Unfortunately, the results were not reliable for this  
267 mixture. Therefore, we had to rely on the information drawn from the experiments with  
268 only one particle type present (Figure 3 and 4). To determine the removal of  $\text{LiFePO}_4$   
269 from the mixture, we performed an additional chemical analysis of the mixture to measure  
270 the iron content. Prior to experiments with both particle types present, we compared the  
271 chemical and reflection based method using  $6 \text{ mLmin}^{-1}$ ,  $500 \text{ kHz}$ , and  $30 V_{\text{pp}}$  with only  
272  $\text{LiFePO}_4$  particles in our suspension. The reflection measurement revealed a signal reduction  
273 of  $19 \pm 1 \%$  (Figure 5B:  $\text{LiFePO}_4$  reflection at  $30 V_{\text{pp}}$ ) whereas the chemical analysis showed  
274 a removal of  $36 \pm 3.0 \%$  (Figure 5A: ratio of 0). Please note, two slightly different signal  
275 reductions of two experimental runs, each representing three experiments, at  $30 V_{\text{pp}}$  and  
276  $6 \text{ mLmin}^{-1}$  are shown (Figure 5B). One set of measurements showed a signal reduction  
277 of  $25 \pm 1.5 \%$ , whereas the other were at  $19 \pm 1 \%$ . We collected the samples for the  
278 chemical analysis from the very same experiments in which we recorded the  $19 \pm 1 \%$  signal  
279 reduction. It is therefore reasonable to compare these two values. The difference between  
280 chemical analysis and reflection measurement can be explained by the different principles  
281 of measurement. While the chemical analysis is measuring the mass of iron, the reflection  
282 does correspond to the particle surface area. Larger  $\text{LiFePO}_4$  particles have high volume  
283 and mass but low specific surface area. Due to their large size and thus higher DEP force,  
284 they are likely to be retained whereas smaller particles are eluted and detected by the  
285 spectrometer. As the smaller particles have a higher specific surface area, they show higher  
286 reflection per mass. Consequently, these two measurement techniques are likely to obtain  
287 different yet valid results. In the supporting information in section S4, we provide more

288 data, including calculations concerning the mass- and surface-weighted distributions of the  
289  $\text{LiFePO}_4$  material, which can explain the deviation.

290 Additionally, we conducted a series of experiments to investigate the influence of the mass  
291 ratio of Actilion and  $\text{LiFePO}_4$  (Figure 5A). The ratio is defined as  $m_{\text{Actilion}}/m_{\text{LiFePO}_4}$ . The  
292 mass ratio does not influence the retention significantly at our set of parameters. Assuming  
293 a complete removal of graphite above  $30 V_{\text{pp}}$  as measured for the pure graphite, we can  
294 assume an almost pure fraction of  $\text{LiFePO}_4$  at the outlet at voltages above  $30 V_{\text{pp}}$  and a  
295 retention of about 35 % to 40 % by mass of the  $\text{LiFePO}_4$  in the filter.

296 The encircled data in point Figure 5A is also shown in Figure 5B in comparison with  
297 results at other voltages. We included the reflection data from Figure 4A of pure Actilion  
298 and  $\text{LiFePO}_4$  for comparison (dotted lines). The chemical analysis again shows an increasing  
299 retention of  $\text{LiFePO}_4$  with voltage (Figure 5B) as it was observed before. Consequently, the  
300 conclusions drawn from the suspensions with only one particle type present remain valid,  
301 meaning that higher voltages than  $30 V_{\text{pp}}$  would not enhance the separation any further.  
302 It is likely that the retention of Actilion in the mixed sample is similar to the previously  
303 measured retention of pure Actilion, mainly because of two effects. First, we could not  
304 observe any saturation effects within our experiments. Even after almost 1000 s of trapping  
305 the signal remained constant (supporting information S3). Second, the addition of  $\text{LiFePO}_4$   
306 particles could even increase the trapping efficiency. This is because trapped particles can  
307 create additional field inhomogeneous that would increase trapping efficiency by forming so-  
308 called pearl chains.<sup>54</sup> Nonetheless, the results would benefit from a further investigation of  
309 the particles and their mixture before and after the separation to show which particle sizes  
310 are retained in the channel and whether there is a cut-off diameter. Also, it needs to be  
311 investigated how residuals on the particles (e.g., binder or electrolyte) or changes in particle  
312 size due to upstream processes interfere with the DEP behavior of the particles and what  
313 space-time yield this method can achieve. However, this is beyond the scope of this study.

314 Concluding, we presented the first study on separation of commercially available electrode

315 active materials using dielectrophoresis. The sorting of the particles could lead towards a  
316 direct recycling step that can be combined with other recycling techniques which than can  
317 reduce the amount of chemicals or energy needed. The results strengthen the assumption that  
318 separability using DEP increases with the difference in particle size. As some cathode active  
319 materials are even smaller than the  $\text{LiFePO}_4$  used in this study,<sup>45</sup> it is worth investigating this  
320 pathway of recycling further. DEP can also be an option for larger cathode active materials,  
321 since the separation could be improved by selective removal of the graphite (several nm  
322 thickness<sup>38</sup>) from the cathode particles while not dissolving the anode graphite in the black  
323 mass completely. This would decrease the conductivity of the cathode particles and result in a  
324 weaker pDEP or even nDEP response of the particles. This would allow material- rather than  
325 size-selective separation which is more robust to size changes in the particle mixture. With  
326 this study, we gave a starting point to direct future research on direct recycling of particle  
327 systems using dielectrophoresis. We further demonstrated the applicability of dielectrophoresis  
328 aside from microfluidic applications.

## 329 **Supporting information**

- 330 • Details of signal processing and background intensity
- 331 • Filter saturation analysis
- 332 • Analysis of influence of particle distribution on measurement procedures
- 333 • Experimental details of the chemical analysis
- 334 • Calculations of Clausius-Mossotti factor

## 335 Abbreviations

336 *CM* - Clausius-Mossotti factor

337 DEP - Dielectrophoresis

338 LIB - Lithium-ion battery

339 nDEP - negative Dielectrophoresis

340 PCB - printed circuit board

341 pDEP - positive Dielectrophoresis

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