

# Sorting lithium-ion battery electrode materials using dielectrophoresis at frequencies of up to 500 kHz

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## Abstract

Lithium-ion batteries (LIBs) are common in everyday life and the demand for their raw materials is increasing. Additionally, spent LIBs should be recycled for achieving a circular economy and supply resources for new LIBs or other products. Especially the recycling of the active material of the electrodes is in the focus of current research. Existing approaches for the recycling (e.g., pyro-, hydrometallurgy or flotation) still have their drawbacks, such as the loss of material, generation of waste, or lack of selectivity. In this study, we test the behavior of commercially available LiFePO<sub>4</sub>

9 and two types of graphite microparticles in a dielectrophoretic high-throughput filter.  
10 Dielectrophoresis is a volume dependent electrokinetic force that is commonly used in  
11 microfluidics but recently also for applications that focus on enhanced throughput. In  
12 our study, graphite particles show significantly higher trapping than  $\text{LiFePO}_4$  particles.  
13 The results indicate that nearly pure fractions of  $\text{LiFePO}_4$  can be obtained with this  
14 technique from a mixture with graphite.

## 15 Introduction

16 Lithium-ion batteries (LIBs) power electrical devices in nearly all parts of modern society.  
17 For example, LIBs are used in portable electronics and electric vehicles. Consequently, the  
18 demand for LIB resources grows.<sup>1</sup> To recover materials of spent LIBs, the recycling of elec-  
19 trodes is a focus of current research. As about one half of the weight of LIBs consists of  
20 the active material of anode and cathode, their recycling is desirable.<sup>2</sup> Cathode active ma-  
21 terials typically are lithium metal oxides (e.g.,  $\text{LiCoO}_2$ ,  $\text{LiFePO}_4$  or  $\text{LiNi}_{1/3}\text{Mn}_{1/3}\text{Co}_{1/3}\text{O}_2$ ),  
22 whereas graphite is common for anodes.<sup>1,2</sup> Anode and cathode consist, among carbon black  
23 as conductive additive and a polymer binder, of a current collector (Cu or Al foil) to which  
24 the active material adheres.<sup>2-4</sup> Current collector and active material can be separated by  
25 both, chemical and mechanical approaches, such as crushing and sieving.<sup>1,3-5</sup> Typically, one  
26 product of these processes is the so-called black mass, a mixture from anode and cathode  
27 active material.<sup>4</sup> Current recycling techniques for black mass are, for example, pyro- or hy-  
28 drometallurgical and focus on the recovery of cathode active material because of its higher  
29 value compared to graphite. Graphite might be lost or burned as energy source within the  
30 recycling process.<sup>1,2,5-7</sup> Yet processes exist where graphite can be recovered. In hydrometal-  
31 lurgical approaches, the lithium metal oxides are dissolved in acid during a leaching step and  
32 recovered in subsequent unit operations. Graphite can simply be recovered by filtration after  
33 the leaching step.<sup>4</sup> But as significant amounts of liquid wastes are produced in this recycling  
34 pathway<sup>8</sup> it would benefit from an efficient sorting step before the leaching to reduce the

35 amount of chemicals needed. As the active materials are essentially microparticles,<sup>9–11</sup> di-  
36 rect recycling using particle separation techniques could play a vital role within the recycling  
37 process to enhance or replace existing recycling approaches of LIBs. One approach which is  
38 well established for particulate systems and capable of handling large amounts of product  
39 is flotation, which was also applied to separate black mass. This works because anode and  
40 cathode material show different wettability.<sup>5,7,12–14</sup> However, according to Neumann et al.,<sup>4</sup>  
41 the process needs to be optimized further as the achievable recovery rates are currently too  
42 low.

43 This paper focuses on developing a novel mechanical approach for separating black mass  
44 using dielectrophoresis (DEP). DEP is the movement of a polarizable particle in an inhomogeneous  
45 electric field. Usually, it is used in the biomedical field and primarily in microfluidic  
46 devices.<sup>15,16</sup> Although DEP is label-free, has high selectivity, and the capability of addressing  
47 nano- to micrometer-scaled particles,<sup>17–19</sup> few studies addressed recycling or the throughput  
48 that would be required for this.<sup>20–25</sup> By using a setup based on printed circuit boards (PCBs),  
49 we assess the behavior of  $\text{LiFePO}_4$  and graphite microparticles and their mixture under the  
50 influence of DEP. To the best of the authors' knowledge the separation of LIB electrode  
51 material using dielectrophoresis has not yet been addressed. This study aims to serve as a  
52 starting point for future research in this field by describing the possibilities and limitations  
53 of DEP as a separation technique for these materials.

## 54 **Materials and Methods**

### 55 **Dielectrophoretic separator**

56 The separator used in this study is an updated version of the one which was evaluated and  
57 published in Ref. 23 and is designed to selectively trap particles when an electric field is  
58 applied. An overview of the device can be seen in Figure 1. The key feature of this device  
59 are two inexpensive ( $< 1\text{€}/\text{pc.}$ ) custom designed PCBs (manufactured by JiaLiChuang

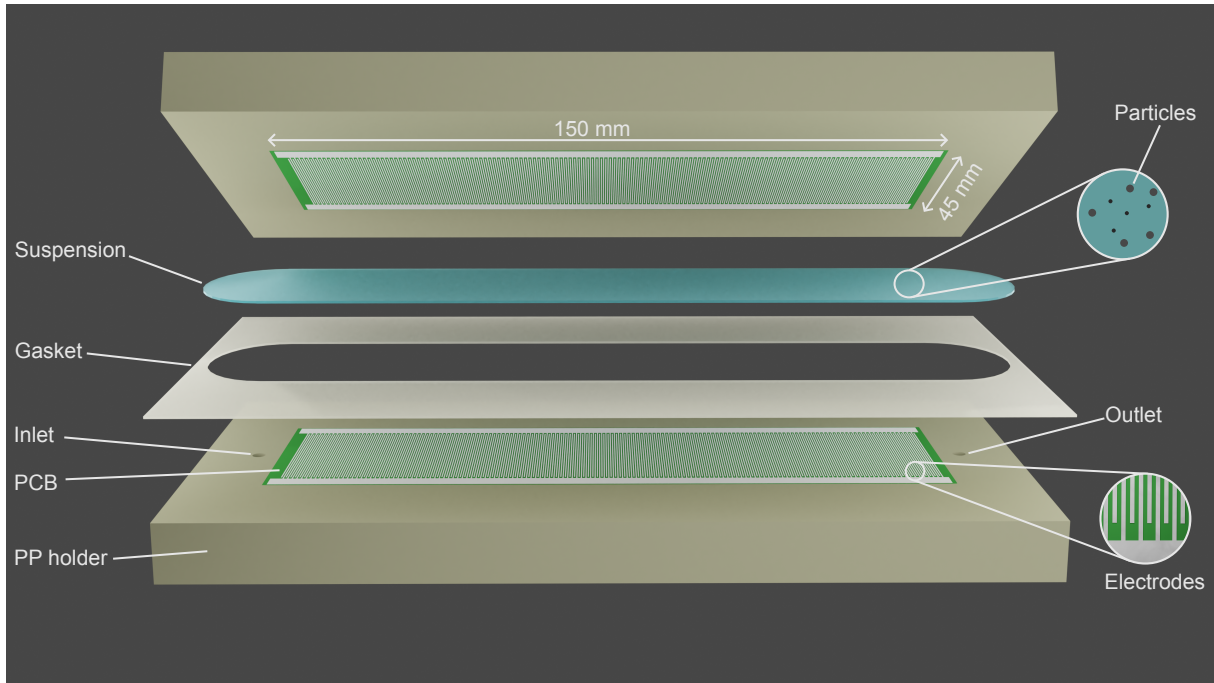


Figure 1: Rendered overview of the separator. The suspension is pumped from inlet to outlet through a channel formed by two printed circuit boards (PCBs), a silicon gasket and the polypropylene (PP) holders. The PCBs feature an interdigitated electrode structure (bottom right insert) that are used to generate a highly inhomogeneous electric field.

60 (HongKong) Co., Limited, China) with a size of  $45 \times 150$  mm, which is slightly different  
 61 from the previous design.<sup>23</sup> The improved design showed better performance with reduced  
 62 PCB size and energy demand. The PCBs are covered by an interdigitated electrode array  
 63 with an electrode width and spacing both being  $250 \mu\text{m}$ . The two PCBs face each other  
 64 and are separated by a  $0.5$  mm silicone gasket. The two PCBs together with the gasket  
 65 form a channel. The electrodes are connected to a power amplifier (F30PV, Pendulum  
 66 Instruments, Sweden) which is capable of providing up to  $75 V_{\text{pp}}$  at maximum current of  $2$  A.  
 67 The sinusoidal signal was generated by a signal generator (Rigol DG4062, Rigol Technologies  
 68 EU GmbH, Germany), monitored using an oscilloscope (Rigol DS2072A, Rigol Technologies  
 69 EU GmbH, Germany) and power analyzer (PPA1510, Newtons4th Ltd, Leicester, United  
 70 Kingdom). The suspension was pumped using a piston pump (Ismatec MCP-CPF IP65  
 71 with pump head FMI 202 QP.Q0.SSY, Cole-Parmer GmbH, Germany).

72 The operating principle is described in detail elsewhere.<sup>23</sup> Briefly, DEP can be an at-



73 tractive force (positive DEP/pDEP) if a particle is better polarizable than the surrounding  
74 medium or a repulsive force (negative DEP/nDEP) when the particle is less polarizable. Pos-  
75 itive DEP guides particle towards local field maxima, whereas nDEP pushes particles away  
76 from them.<sup>15</sup> This can lead to a separation as was previously shown several times.<sup>23,26,27</sup>  
77 Whether a particle experiences pDEP or nDEP depends on the real-part of the Clausius-  
78 Mossotti factor ( $CM$ ), which is defined as<sup>15</sup>

$$\text{Re}(CM) = \text{Re} \left( \frac{\tilde{\epsilon}_p - \tilde{\epsilon}_m}{\tilde{\epsilon}_p + 2\tilde{\epsilon}_m} \right), \quad (1)$$

79 with the complex permittivity  $\tilde{\epsilon} = \epsilon_0 \epsilon_r - i \frac{\sigma}{\omega}$ . The complex permittivity incorporates not only  
80 the permittivity  $\epsilon$  but also the angular frequency of the electric field  $\omega$  and the conductivity  
81 of a material  $\sigma$ .  $\text{Re}(CM)$  is bound between  $-0.5$  and  $1.0$  and is negative in case of nDEP  
82 and positive in case of pDEP. Finally, the DEP force  $\mathbf{F}_{\text{DEP}}$  for a spherical and homogeneous  
83 particle can be approximated as

$$\mathbf{F}_{\text{DEP}} = 2\pi r_p^3 \epsilon_m \text{Re}(CM) \nabla |\mathbf{E}_{\text{rms}}|^2 \quad (2)$$

84 with  $r_p$ , the radius of the particle, the electric field,  $\mathbf{E}_{\text{rms}}$ , and the permittivity of the sur-  
85 rounding medium,  $\epsilon_m$ . Conductive particles in a medium with low conductivity, as used  
86 in this study, will usually experience pDEP.  $\mathbf{F}_{\text{DEP}}$  is not only depending on the particle  
87 and medium polarizability but also on the particle volume ( $r_p^3$ ) which is important in the  
88 following.

## 89 **Particles**

90 The particles investigated here all are commercially available. We chose  $\text{LiFePO}_4$  (Nanografi  
91 Nano Teknoloji AS, Turkey) as a cathode material, not only because it is widely used for  
92 LIBs but also because it is considered to have low toxicity, which makes it more convenient  
93 to work with.<sup>11,28,29</sup>  $\text{LiFePO}_4$  as cathode material is carbon coated to enhance its otherwise

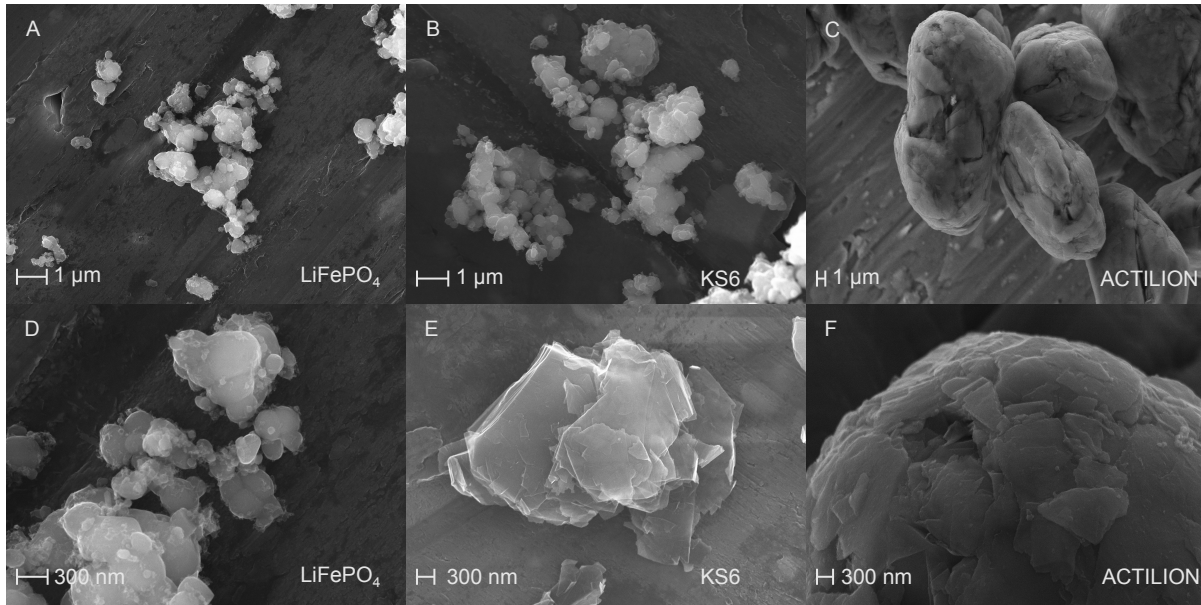


Figure 2: SEM images of  $\text{LiFePO}_4$  (A&D), KS6 synthetic graphite (B&E) and C-ENERGY<sup>TM</sup> Actilion GHDR 15-4 (C&F) microparticles. The scale bar in the top row equals 1  $\mu\text{m}$  and 300 nm in the bottom row. Please note that the magnification and consequently the scale bar varies in size.

94 poor conductivity (about  $10 \text{ nS/cm}^{-1}$ ). This leads, according to the distributor, to an  
 95 electrical conductivity of  $0.88 \text{ S/m}$ .<sup>30,31</sup> The used  $\text{LiFePO}_4$  shows a distributed particle size  
 96 from several hundred nm to a few  $\mu\text{m}$  (Table 1, Figure 2 A&D). This is in the range of sizes  
 97 mentioned in the literature<sup>32-35</sup> and also in the range of the size reported for some other  
 98 cathode materials.<sup>36</sup> Additionally, two types of graphite particles were selected. Timrex  
 99 KS6 (MSE Supplies LLC, USA) is a synthetic graphite with high purity which can be used  
 100 as conductive additive for anodes and cathodes. According to the manufacturer (Imerys  
 101 Graphite & Carbon, Switzerland), it is larger than the  $\text{LiFePO}_4$  particles (Table 1, Figure  
 102 2 B&E). The second type of graphite C-ENERGY<sup>TM</sup> Actilion GHDR 15-4 (provided by  
 103 Imerys Graphite & Carbon, Switzerland), here referred to as Actilion, is an active material  
 104 for anodes of LIBs and significantly larger than the other two materials (Table 1, Figure  
 105 2 C&F). The larger size of anode graphite was also described in the literature.<sup>10,11,35</sup> Both  
 106 graphite and LFP are highly conductive compared to the suspension and thus will show  
 107 pDEP at all frequencies used in this study. Therefore, all particles will move towards field

108 maxima which are located at the edges of the electrode array on the PCBs. As the sizes of  
 109 the particles here diverge significantly, we aim to exploit the linear volume dependence of  
 110  $\mathbf{F}_{\text{DEP}}$  to achieve a separation.

Table 1: Parameters describing the size distribution of the used particles

Particle	$d_{10} / \mu\text{m}$	$d_{50} / \mu\text{m}$	$d_{90} / \mu\text{m}$
LiFePO <sub>4</sub>	0.6	1.5	6.0
KS6	1.5	3.4	6.1
Actilion	13	17	23

## 111 Measurement system

112 Two methods were used to measure the particle separation. Qualitatively, the total particle  
 113 concentration was measured by white-light reflection in real-time at the outlet. Quanti-  
 114 tatively, the LiFePO<sub>4</sub> concentration was further evaluated using photometric detection of  
 115 dissolved iron mass. The reflection measurement system is described in Ref. 23. Briefly, it  
 116 consists of a spectrometer (Silver nova, StellarNet, Inc., USA) and a flow cuvette (176-765-  
 117 85-40 and 176-760-85-40, Hellma GmbH & Co. KG, Germany). A white light source (XCite  
 118 120 PC, Excelitas Technologies Corp., USA) is connected in 90° with respect to the light  
 119 guide of the spectrometer. Particles in the flow cuvette will scatter the light and produce  
 120 a signal that can be recorded by the spectrometer. For size-distributed particle systems,  
 121 it is important to keep in mind that the reflection intensity varies with particle size. For  
 122 spheres in the size range of the particles used here and the wavelength of the light source,  
 123 the scattering intensity is proportional to  $r_p^2$ .<sup>37</sup> As the particles here are not perfect spheres  
 124 (Figure 2), the signal recorded by the spectrometer does not provide the information of the  
 125 number or mass of eluted particles, which is different compared to monodisperse particulate  
 126 systems as in Ref. 23 and 20. This certainly is a downside of the reflection measurement  
 127 setup. We thus use the measured reflective light intensity reduction at the outlet as a qual-  
 128 itative real-time indicator of particle retention. To measure the retention of LiFePO<sub>4</sub> in the  
 129 filter, we used a chemical procedure which allows a photometric determination of the iron

130 mass. The procedure was derived from DIN 38406 (see supporting information S5). Briefly,  
131 the  $\text{LiFePO}_4$  particles are dissolved in an acid and the iron content is determined using a  
132 complexing agent and performing a photometric measurement afterward.<sup>38</sup>

## 133 **Experimental procedure**

134 Experiments were carried out in a low-conductivity medium (2.1  $\mu\text{S}/\text{cm}$ ) consisting of pure  
135 water (Omniatap 6 UV/UF, stakpure GmbH, Germany), 0.01 vol.% Tween 20 (Sigma–Aldrich,  
136 Germany), and KCl to adjust the conductivity. To create particle stock suspensions, the par-  
137 ticles were suspended in an 1 vol.% aqueous Tween 20 suspension with 4 g/L for  $\text{LiFePO}_4$   
138 and KS6 and 12 g/L for Actilion. The  $\text{LiFePO}_4$  suspension was renewed every three days as  
139 Li is known to dissolve to a low extend into aqueous solutions,<sup>39</sup> and we wanted to exclude  
140 this effect from our experiments. Prior to the experiments, we sonicated the particle stock  
141 suspensions and added 0.22 vol.% of it, for  $\text{LiFePO}_4$  and KS6, into the medium for the ex-  
142 periments. In order to achieve a sufficient reflection signal, we had to increase the Actilion  
143 concentration, resulting in a  $10\times$  higher total mass of Actilion in the final suspension com-  
144 pared to the other two particle types. The reason behind this might be lower specific surface  
145 area of the larger Actilion particles and thus lower reflectance per added mass.

146 The suspensions were stirred throughout the entire experiment. To subtract the back-  
147 ground signal, we recorded the intensity signal daily with no particles present (supporting  
148 information S2). At the beginning of the experiments we measured the initial reflection  
149 signal of the particle suspension for 30 s. At 30 s the electric field was turned on for 270 s.  
150 After the voltage was turned off, the experiment was further monitored until the initial in-  
151 tensity was obtained again. Sometimes, the initial signal was not fully reached due to effects  
152 such as sedimentation or bubble adhesion in the flow-through cuvette. As a consequence we  
153 flushed the entire setup at a high flow rate after every two experiments. Every data point  
154 represents three experiments. Equation 1 in section S1 of the supplement details how the  
155 signal reduction is calculated.

156 To chemically determine the retention of the  $\text{LiFePO}_4$  particles, we collected 4 mL of  
 157 suspension in a 5 mL container. The samples were taken at the beginning of the experiment,  
 158 starting after 5 s and during the trapping, starting after 200 s. In order to obtain a sufficient  
 159 sample volume at the beginning of the experiment, the voltage was turned on after 60 s.

160 All data from the reflection measurements, the evaluation script (MATLAB, details see  
 161 supporting information S1) and PCB manufacturing data are uploaded to an online reposi-  
 162 tory (Ref. 40).

## 163 Results and Discussion

### 164 Frequency dependent behavior up to 500 kHz

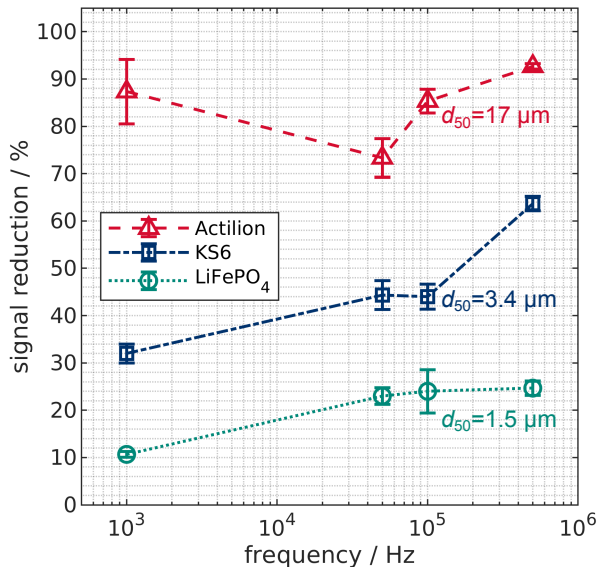


Figure 3: Frequency dependency of the signal reduction of Acilion, KS6 and  $\text{LiFePO}_4$  suspensions at  $6 \text{ mLmin}^{-1}$  and  $30 \text{ V}_{\text{pp}}$ . Frequencies were varied between 1 kHz and 500 kHz.

165 All particles in this study are conductive and thus should show pDEP. To test this  
 166 hypothesis, we conducted experiments at  $30 \text{ V}_{\text{pp}}$  from 1 kHz to 500 kHz at a volume flow of  
 167  $6 \text{ mLmin}^{-1}$  with only one particle type present per experiment (Figure 3). Higher frequencies

168 were not applicable in this setup and the selected voltage, because the required current would  
169 exceed the maximum of the amplifier. For all particles the trapping efficiency (measured  
170 qualitatively in terms of reduction of reflective light intensity signal, called signal reduction)  
171 was highest at 500 kHz and significantly higher than at lower frequencies. This might be  
172 because disturbing electrokinetic effects like AC electroosmosis can be dominant at lower  
173 frequencies.<sup>41</sup> Furthermore, significant difference in the signal reduction becomes apparent  
174 when comparing the particle types. This is likely caused by the differences in particles size  
175 as DEP scales with particle volume (Equation 2). For example, at 30  $V_{pp}$  and 500 kHz,  
176 Actilion shows a high signal reduction of  $92.67 \pm 0.58$  % but the signal of  $\text{LiFePO}_4$  is only  
177 reduced by  $24.67 \pm 1.53$  %. To further investigate the behavior of the particles, we selected  
178 500 kHz as frequency for all subsequent experiments, because the performance of the device  
179 is the highest at this frequency and DEP the dominating force. The application of 500 kHz  
180 also demonstrates that frequencies in this range can be applied in a high throughput device.  
181 A higher possible frequency can be beneficial when designing the process as with increasing  
182 frequency the polarizability can alter and enable a separation. In a previous study we could  
183 show that retention due to nDEP is small ( $< 10$  %) in such a setup and therefore is not the  
184 reason for our observations.<sup>23</sup>

## 185 **Influence of voltage and volume flow**

186 As second step, we investigated the influence voltage on signal reduction from 5 to 75  $V_{pp}$   
187 at 6  $\text{mLmin}^{-1}$  (Figure 4A) and 10  $\text{mLmin}^{-1}$  (Figure 4B). At both flow rates, all particles  
188 show an increased signal reduction or particle retention with increasing voltage. This is in  
189 line with the approximation of the DEP force (Equation 2). Additionally, increasing volume  
190 flow decreases the signal reduction. This is due to the increased viscous drag and decreased  
191 residence time in the setup at the higher flow rate. The data at 6  $\text{mLmin}^{-1}$  and 30  $V_{pp}$   
192 is the same as in Figure 3, except for Actilion. Here, we used a different flow cuvette for  
193 this measurements to prevent sedimentation. However, the results are quite similar (here

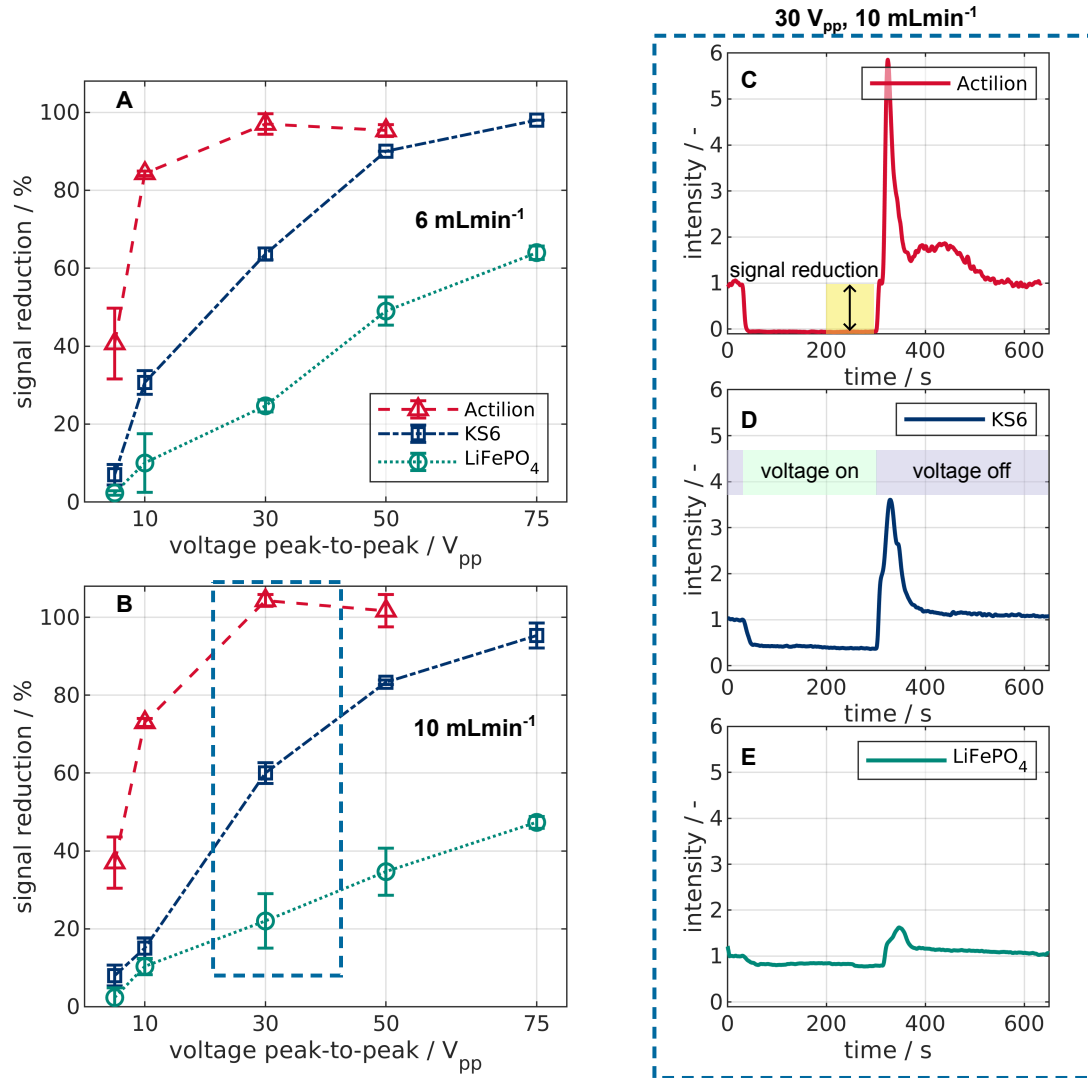


Figure 4: Voltage and volume flow dependency of the signal reduction for Acitlion, KS6 and LiFePO<sub>4</sub> suspensions at a frequency of 500 kHz. The behavior was evaluated between 5 and 75 V<sub>pp</sub> at 6 mLmin<sup>-1</sup> (A) and 10 mLmin<sup>-1</sup> (B). As example, normalized reflection intensities over time for all materials at 30 V<sub>pp</sub> and 10 mLmin<sup>-1</sup> are also shown (C-E). For all experiments, the signal reduction was measured between 200 and 300 s (C). The voltage was applied after 30 s for 270 s (D).

194  $97 \pm 2.65$  % compared to  $92.67 \pm 0.58$  %). Figure 4 C-E shows intensity plots over time for all  
195 particles at  $30 V_{pp}$  and  $10 \text{ mLmin}^{-1}$ . Three things become apparent from Figure 4. First,  
196 the signal reduction of Actilion is significantly higher than that of  $\text{LiFePO}_4$ . For example,  
197 at  $30 V_{pp}$  and  $10 \text{ mLmin}^{-1}$  (Figure 4 B,C and E), the signal reduction of Actilion is over  
198 four times higher than it is for  $\text{LiFePO}_4$ . Here, the recorded intensity for Actilion is close  
199 to zero, indicating a complete removal. The relative difference of the signal reduction of  
200  $\text{LiFePO}_4$  and Actilion, however, decreases with increasing voltage (Figure 4A and B). Likely,  
201 this is because Actilion is already almost completely removed at voltages over  $30 V_{pp}$  at both  
202 flow rates, whereas  $\text{LiFePO}_4$  removal increases with voltage from 0 to  $75 V_{pp}$ . Second, KS6  
203 also shows significant trapping and gets fully removed at about  $75 V_{pp}$  at both flow rates.  
204 Third, the reflection measurements can create signal reduction slightly higher than 100 %  
205 which is linked to the subtraction of the background signal and was observed before.<sup>23</sup> The  
206 highest recorded value was  $104.33 \pm 1.53\%$  at  $10 \text{ mLmin}^{-1}$  and  $30 V_{pp}$ . As the deviation is  
207 explainable (supporting information S2), relatively small, and showing a complete removal  
208 of Actilion, we do not consider this problematic.

209 In summary, the size, voltage, and volume flow dependency of the signal reduction for  
210 these particles was as expected. In addition, we observed an almost complete removal of  
211 Actilion from the suspension starting at  $30 V_{pp}$ . For mixtures of  $\text{LiFePO}_4$  and Actilion,  
212 this would correspond to a pure fraction of  $\text{LiFePO}_4$  at the outlet and an enrichment of  
213 Actilion within the filter. Higher voltages than  $30 V_{pp}$  would not lead to a significantly  
214 increased trapping of Actilion but to more retained  $\text{LiFePO}_4$ . Therefore, we selected  $30 V_{pp}$   
215 for separation experiments of Actilion and  $\text{LiFePO}_4$ .

## 216 **Behavior in a mixture of graphite and $\text{LiFePO}_4$**

217 As a final step, we investigated the separability of a mixture of  $\text{LiFePO}_4$  and Actilion.  
218 We did not include KS6 because conductive additives are only around 4 % of the battery  
219 mass.<sup>2</sup> It would further increase the difficulty of analyzing the results because the reflection



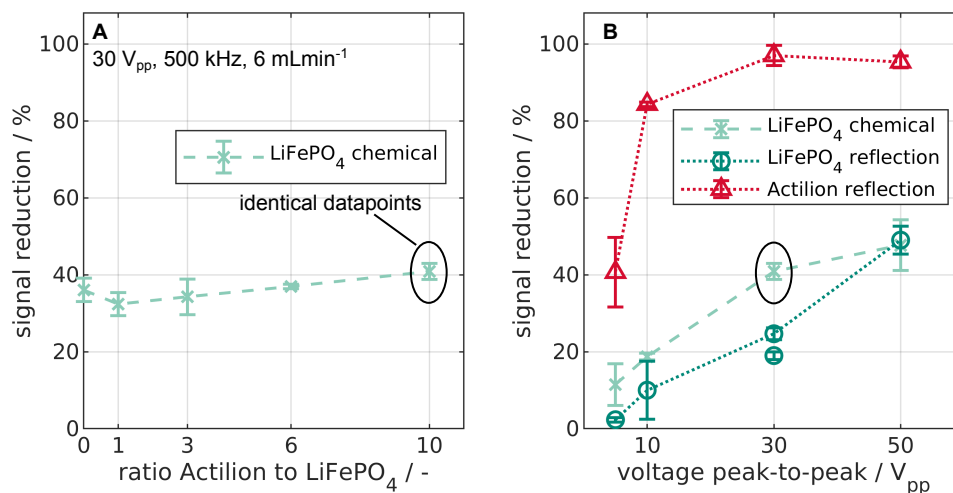


Figure 5: A: Variation of the mass ratio of LiFePO<sub>4</sub> and Actilion graphite particles in the suspension at 30 V<sub>pp</sub>, 500 kHz and 6mLmin<sup>-1</sup>. B: Comparison of reflection measurements of suspensions with only one particle type present (dotted lines) and the chemical analysis of LiFePO<sub>4</sub> removal from a mixture with 10 times more mass of Actilion than LiFePO<sub>4</sub> (dashed line).

220 measurement is not material sensitive. We tried to calculate separate reflection spectra for  
 221 each component by superposition of the reflection spectra of pure LiFePO<sub>4</sub> and Actilion,  
 222 as they are slightly different. For fluorescent particles this can be achieved by coupling  
 223 these reference spectra with a global optimization to calculate separate intensities over time  
 224 distributions as described in Ref. 22. Unfortunately, the results were not reliable for this  
 225 mixture. Therefore, we had to rely on the information drawn from the experiments with  
 226 only one particle type present (Figure 3 and 4). To determine the removal of LiFePO<sub>4</sub>  
 227 from the mixture, we performed an additional chemical analysis of the mixture to measure  
 228 the iron content. Prior to experiments with both particle types present, we compared the  
 229 chemical and reflection based method using 6 mLmin<sup>-1</sup>, 500 kHz, and 30 V<sub>pp</sub> with only  
 230 LiFePO<sub>4</sub> particles in our suspension. The reflection measurement revealed a signal reduction  
 231 of  $19 \pm 1$  % (Figure 5B: LiFePO<sub>4</sub> reflection at 30 V<sub>pp</sub>) whereas the chemical analysis showed  
 232 a removal of  $36.1 \pm 3.04$  % (Figure 5A: ratio of 0). Please note, two slightly different signal  
 233 reductions of two experimental runs, each representing three experiments, at 30 V<sub>pp</sub> and  
 234 6 mLmin<sup>-1</sup> are shown (Figure 5B). One set of measurements showed a signal reduction

235 of  $24.7 \pm 1.5$  %, whereas the other were at  $19 \pm 1$  %. We collected the samples for the  
236 chemical analysis from the very same experiments in which we recorded the  $19 \pm 1$  % signal  
237 reduction. It is therefore reasonable to compare these two values. The difference between  
238 chemical analysis and reflection measurement can be explained by the different principles  
239 of measurement. While the chemical analysis is measuring the mass of iron, the reflection  
240 does correspond to the particle surface area. Larger  $\text{LiFePO}_4$  particles have high volume  
241 and mass but low specific surface area. Due to their large size and thus higher DEP force,  
242 they are likely to be retained whereas smaller particles are eluted and detected by the  
243 spectrometer. As the smaller particles have a higher specific surface area, they show higher  
244 reflection per mass. Consequently, these two measurement techniques are likely to obtain  
245 different yet valid results. In the supporting information in section S4, we provide more  
246 data, including calculations concerning the mass- and surface-weighted distributions of the  
247  $\text{LiFePO}_4$  material, which can explain the deviation.

248 Additionally, we conducted a series of experiments to investigate the influence of the mass  
249 ratio of Actilion and  $\text{LiFePO}_4$  (Figure 5A). The ratio is defined as  $m_{\text{Actilion}}/m_{\text{LiFePO}_4}$ . The  
250 mass ratio does not influence the retention significantly at our set of parameters. Assuming  
251 a complete removal of graphite above  $30 V_{\text{pp}}$  as measured for the pure graphite, we can  
252 assume an almost pure fraction of  $\text{LiFePO}_4$  at the outlet at voltages above  $30 V_{\text{pp}}$  and a  
253 retention of about 35 % to 40 % by mass of the  $\text{LiFePO}_4$  in the filter.

254 The encircled data in point Figure 5A is also shown in Figure 5B in comparison with  
255 results at other voltages. We included the reflection data from Figure 4A of pure Actilion  
256 and  $\text{LiFePO}_4$  for comparison (dotted lines). The chemical analysis again shows an increasing  
257 retention of  $\text{LiFePO}_4$  with voltage (Figure 5B) as it was observed before. Consequently, the  
258 conclusions drawn from the suspensions with only one particle type present remain valid,  
259 meaning that higher voltages than  $30 V_{\text{pp}}$  would not enhance the separation any further.  
260 It is likely that the retention of Actilion in the mixed sample is similar to the previously  
261 measured retention of pure Actilion, mainly because of two effects. First, we could not

262 observe any saturation effects within our experiments. Even after almost 1000 s of trapping  
263 the signal remained constant (supporting information S3). Second, the addition of  $\text{LiFePO}_4$   
264 particles could even increase the trapping efficiency. This is because trapped particles can  
265 create additional field inhomogeneous that would increase trapping efficiency by forming  
266 so-called pearl chains.<sup>42</sup> Nonetheless, the results would benefit from a further investigation  
267 of the particles and their mixture before and after the separation to show which particle  
268 sizes are retained in the channel and whether there is a cut-off diameter. Also, it needs to  
269 be investigated how residuals on the particles (e.g., binder or electrolyte) interfere with the  
270 DEP behavior of the particles and what space-time yield this method can achieve. However,  
271 this is beyond the scope of this study.

272 Concluding, we presented the first study on separation of commercially available electrode  
273 active materials using dielectrophoresis. The sorting of the particles could lead towards a  
274 direct recycling step that can be combined with other recycling techniques which than can  
275 reduce the amount of chemicals or energy needed. The results strengthen the assumption that  
276 separability using DEP increases with the difference in particle size. As some cathode active  
277 materials are even smaller than the  $\text{LiFePO}_4$  used in this study,<sup>36</sup> it is worth investigating this  
278 pathway of recycling further. DEP can also be an option for larger cathode active materials,  
279 since the separation could be improved by selective removal of the graphite (several nm  
280 thickness<sup>30</sup>) from the cathode particles while not dissolving the anode graphite in the black  
281 mass completely. This would decrease the conductivity of the cathode particles and result  
282 in weaker pDEP or even nDEP response of the particles and therefore allows material-  
283 rather than size-selective separation. With this study, we gave a starting point to direct  
284 future research on direct recycling of particle systems using dielectrophoresis. We further  
285 demonstrated the applicability of dielectrophoresis aside from microfluidic applications.

## 286 Abbreviations

287 *CM* - Clausius-Mossotti factor

288 DEP - Dielectrophoresis

289 LIB - Lithium-ion battery

290 nDEP - negative Dielectrophoresis

291 PCB - printed circuit board

292 pDEP - positive Dielectrophoresis

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