

1 Standardized Measurement of Surface Dry Particle Thickness for Walkway Slip Resistance

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7 Keywords: slip resistance, floors, tribometry, coefficient of friction, particles, rubbing

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29 Abstract

30 Slip and fall incidents remain a critical safety concern in residential and occupational settings.
31 While considerable research has focused on wet contamination, the role of dry contaminants in
32 reducing floor friction has been less explored. This study establishes a standardized methodology
33 for measuring dry particle thickness and investigates the effects of recombining dry contaminants
34 on the coefficient of friction (COF). Using a modified tribometer and custom 3D-printed combs
35 (127 μ m, 254 μ m, and 508 μ m depths), iodized salt was applied to a high-gloss tile, and COF was
36 measured under recombined and non-recombined conditions. Results indicated that recombining
37 significantly lowered COF, whereas non-recombined conditions did not differ from the
38 uncontaminated tile, highlighting the necessity of recombining to accurately assess slip resistance.
39 This study presents a cost-effective approach to slip-resistance testing, with implications for
40 forensic investigations, industry safety standards, and workplace hazard assessments.

41 Keywords: **SLIP RESISTANCE, FLOORS, TRIBOMETRY, COEFFICIENT OF**
42 **FRICITION, PARTICLES, RUBBING**

43 Highlights

- 44 • Introduces a standardized method to measure dry particle thickness for slip resistance
45 assessment.
- 46 • Demonstrates that recombining dry contaminants reduces the coefficient of friction (COF)
47 by 19.28% compared to not recombining.
- 48 • Provides a cost-effective, practical approach for forensic investigations and workplace
49 hazard assessments.

51 Introduction

52 Slips and falls are considered a serious hazard in the home and the workplace [1,2]. The
53 majority of research has focused on slip incidents induced by water contamination [3–5], oil
54 contamination [6–12], or moving platforms [13–17]. Few studies have investigated the role of dry
55 contaminants in slip incidents as a potential mechanism that reduces the friction between the foot-
56 floor interface [18,19]. Understanding how dry contaminants affect the coefficient of friction
57 (COF) can help inform maintenance standards for determining the slip resistance of floors.

58 Previous studies assessing floor friction under wet conditions have ensured that a
59 continuous film of water was present before the test-foot of the tribometer contacted the tile surface
60 [3,4,20,21]. This is important as tribometers such as the Mark IIIb, English XL, and the KSS
61 pendulum use test foos that strike the contaminated floor and push contaminants away from the
62 test foot, and require multiple consecutive tests to determine slip resistance. Similarly, devices like
63 the drag sled and BOT-3000e use test foos that drag across the floor which can also push
64 contaminants off of the surface. This methodological approach of maintaining a continuous film
65 of contaminant after each test is important as it replicates human gait behavior in real-world
66 scenarios, where individuals step onto a liquid contaminant rather than directly onto the flooring
67 substrate. Ensuring a uniform liquid layer at the point of contact improves the validity of friction
68 measurements by accurately representing the slip potential encountered in actual walking
69 conditions.

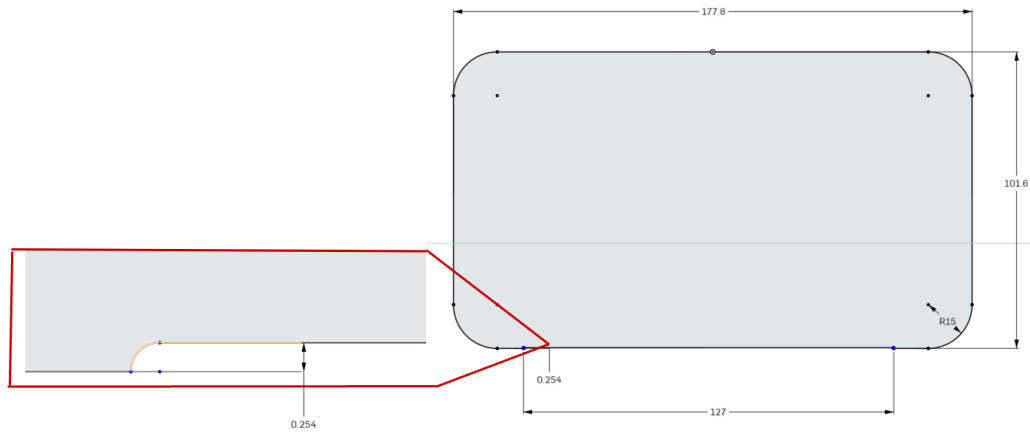
70 The methodology for controlling dry substances during tribometer testing has not been
71 established. Methodologically, one study used 10g of 5 different particle sizes that were distributed
72 with a special comb [19]. Furthermore, this study did not replenish or recomb the particles after
73 the tribometer test foot struck the dry contaminants. This likely affects the results, as the tribometer

74 test foot may displace particles or change their thickness on the tested flooring surface. Another
75 study used 500 μ M to 2000 μ M depth combs for different thickness levels of particles that ranged
76 from 5 to 200 μ M in size [18]. This methodology did not state whether the particles were recombined
77 (re-leveled) to ensure the thickness levels were the same at each strike.

78 Previous studies either did not replenish the particles after tribometer strikes or lacked a
79 standardized method for ensuring consistent thickness levels. As such, the purpose of this study
80 was to establish a standardized methodological approach to measuring the thickness of particle
81 level and determine if there is an effect of recombining dry contaminants after each tribometer test,
82 and thickness level of particulate matter on the coefficient of friction. We hypothesized that: (1)
83 thinner layers of particulate matter would reduce COF more than thicker layers due to increased
84 surface coverage, and (2) recombining would further decrease COF by ensuring consistent
85 contaminant distribution after each tribometer strike. The results of this paper will provide a more
86 standardized and economical approach to measuring dry contaminants' effect on slip resistance.

87 Methodology

88 One 12'' x 24'' white polished porcelain high-gloss tile was utilized for this study (Belucci
89 Bianca, SKU 10096621, Brazil). A modified Ender-3 V2 3D printer (Creality, Shenzhen, China)
90 with a 0.2mm nozzle utilized polylactic acid material to develop specialized combs of varying
91 depths to control the thickness layer of particles on the tile. Three specialized combs were created
92 with a depth of 127 micrometers, 254 micrometers and 508 micrometers, respectively (Fig. 1).
93 Iodized table salt was used for the dry contaminants in this study. A calibrated and validated Mark
94 III tribometer (Slip-Test, LLC, Philadelphia, PA, USA) was utilized to test the coefficient of
95 friction.



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97 Figure 1. A schematic of the 254 μM comb. The red box shows a zoomed in perspective of the
 98 depth of the comb that allows 254 μM of material under it.

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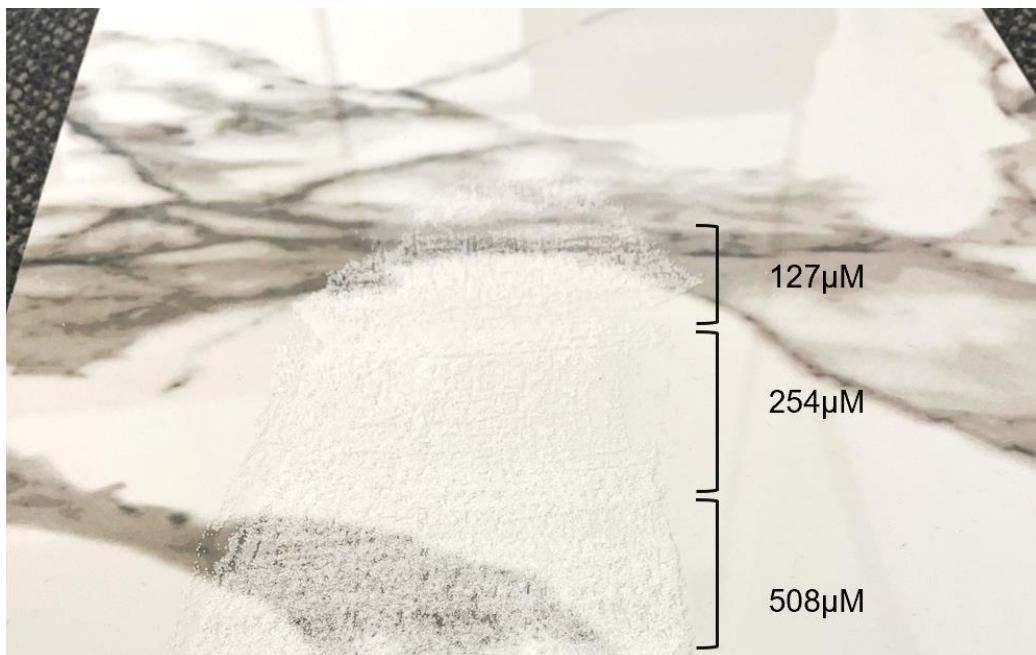
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101 Figure 2. The three combs used in this study, 508 μM (left), 254 μM (middle) and 127 μM
 102 (right). The light coming from behind the combs allows light to pass under the comb to view the
 103 different comb depths.

104 Procedures

105 For baseline testing, the coefficient of friction of the uncontaminated tile was measured in
 106 four directions by three researchers totaling 12 COF recordings. Iodized salt was evenly spread
 107 using the 127 μM comb held vertical and dragged horizontally across the tile (Fig. 3). The
 108 tribometer was placed over the leveled iodized salt so the test foot would strike the even layer. The

109 tribometer performed multiple trials, with the test foot repeatedly striking the contaminant, to
110 obtain a stable slip resistance measurement. For the recombining condition, the contaminant was
111 recombined between each test foot strike with the respective depth so there was a consistent level
112 each time the tribometer made a test foot strike. The coefficient of friction was tested in four
113 orthogonal directions on the tile and the COF was reported for each direction as done in prior
114 studies [3,4,20,22]. This process was repeated for 254 μ M and 508 μ M of the iodized salt. Three
115 researchers tested each contaminant, and each thickness level of the particle, on the tile in four
116 directions, yielding a total of 12 samples per thickness of the contaminant. For the no recombining
117 condition, the contaminant was not recombined between each test foot strike with the respective
118 depth and the dry contaminants distribution after each strike was not considered. The coefficient
119 of friction was tested in four orthogonal directions on the tile and the COF was reported for each
120 direction. This process was repeated for 254 μ M and 508 μ M of the iodized salt. Three researchers
121 tested each contaminant, and each thickness level of the particle, on the tile in four directions,
122 yielding a total of 12 samples per thickness of the contaminant.



124 Figure 3. A photograph showing the three depth surfaces (127 μ M, 254 μ M and 508 μ M) of the
125 iodized salt on the tile.

126 Analysis

127 Statistical treatments were conducted with SPSS (IBM SPSS Statistics for Windows,
128 Version 29.0.2.0, Armonk, NY: IBM Corp). A one-way repeated measures ANOVA was
129 conducted followed by post hoc pairwise comparisons with a Bonferroni correction to determine
130 if the coefficient of friction was influenced by the thickness of the particle level and recombining.
131 Significance was set to $\alpha < 0.05$.

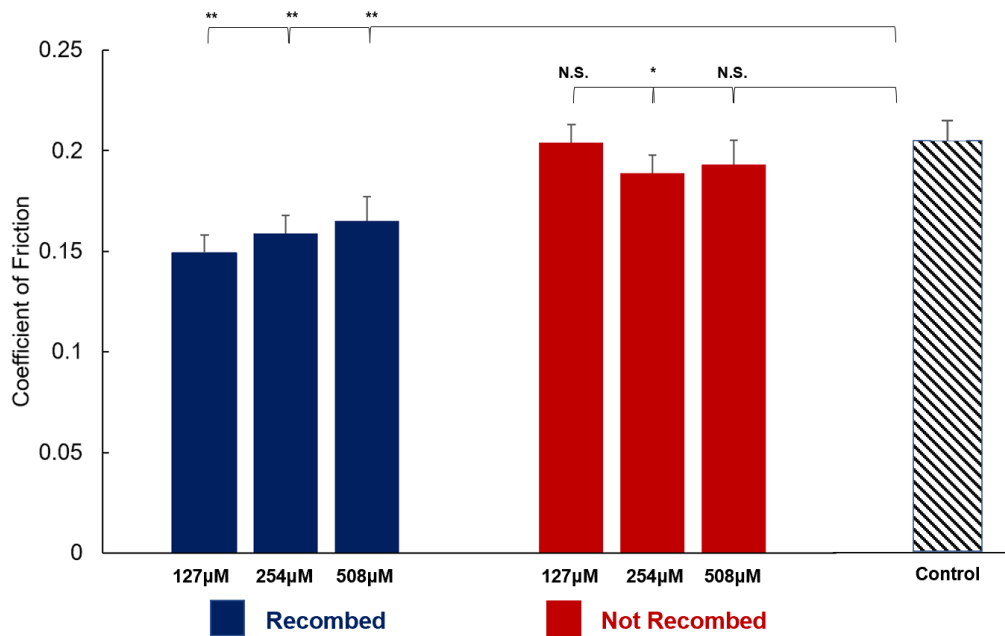
132 Results

133 A one-way repeated measures ANOVA was conducted to evaluate the effect of combing and
134 particle thickness on the coefficient of friction (COF) of a surface contaminated with dry particles.
135 The seven experimental conditions included: recombined 127 μ m, recombined 254 μ m, recombined
136 508 μ m, not recombined 127 μ m, not recombined 254 μ m, not recombined 508 μ m, and an uncontaminated
137 control condition.

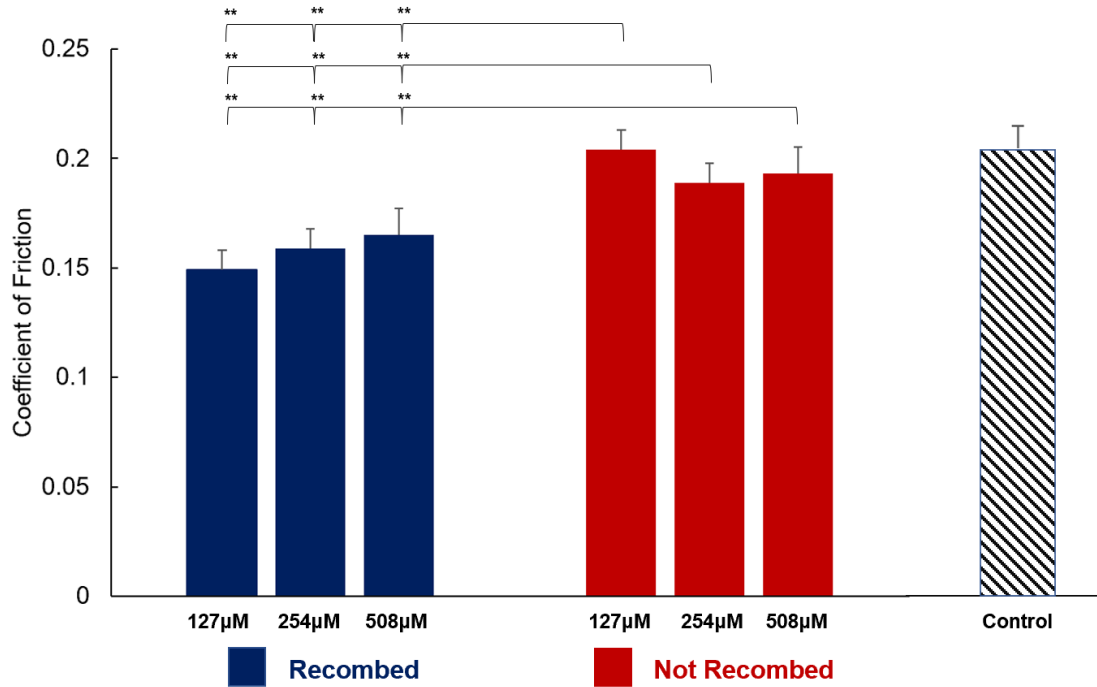
138 The mean COF values for each condition were as follows: recombined 127 μ m (M = 0.149, SD =
139 0.0079), recombined 254 μ m (M = 0.159, SD = 0.0090), recombined 508 μ m (M = 0.165, SD = 0.0100),
140 not recombined 127 μ m (M = 0.204, SD = 0.0178), not recombined 254 μ m (M = 0.189, SD = 0.0079),
141 not recombined 508 μ m (M = 0.193, SD = 0.0123), and the control (M = 0.208, SD = 0.0097).

142 Mauchly's test of sphericity was non-significant ($W = 0.048$, $\chi^2(20) = 26.63$, $p = 0.170$), indicating
143 that the assumption of sphericity was met, and standard F-tests were used. The repeated measures
144 ANOVA revealed a significant main effect of condition on COF ($F(6,66) = 51.32$, $p < 0.001$, $\eta^2 =$
145 0.823), indicating that at least one condition differed significantly from the others.

146 Pairwise comparisons with Bonferroni correction were conducted. All recombed contaminated
 147 conditions had significantly lower COF than the control condition ($p < 0.001$, Fig. 4). There were
 148 no significant differences in COF between the control tile and recombed conditions of 127 μm (p
 149 = 1.00) and 508 μm ($p = .394$, Fig. 4). The control tile exhibited significantly greater COF than the
 150 not recombed 254 μm ($p = 0.02$, Fig. 4). Not recombed 127 μm , 254 μm , and 508 μm had a
 151 significantly higher COF than all recombed conditions ($p < 0.001$, Fig. 5). Within the recombed
 152 conditions, 127 μm had a significantly lower COF than 500 μm ($p = 0.01$, Fig. 6). Among not
 153 recombed conditions, there were no significant COF differences between 127 μm and 254 μm ($p =$
 154 0.493, Fig. 6), 127 μm and 508 μm ($p = 1.00$, Fig. 6), and 254 μm and 508 μm ($p = 1.00$, Fig. 6).



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 156 Figure 4. COF values for recombed (blue) and not recombed (red) particle thicknesses at
 157 127 μM , 254 μM and 508 μM compared to the tile's COF with no dry substance (control). Error
 158 bars indicate standard deviation. ** denotes significant differences at $p < 0.001$ and * denotes
 159 significant at $p = 0.02$. N.S. denotes Not Significant at $p < 0.05$.



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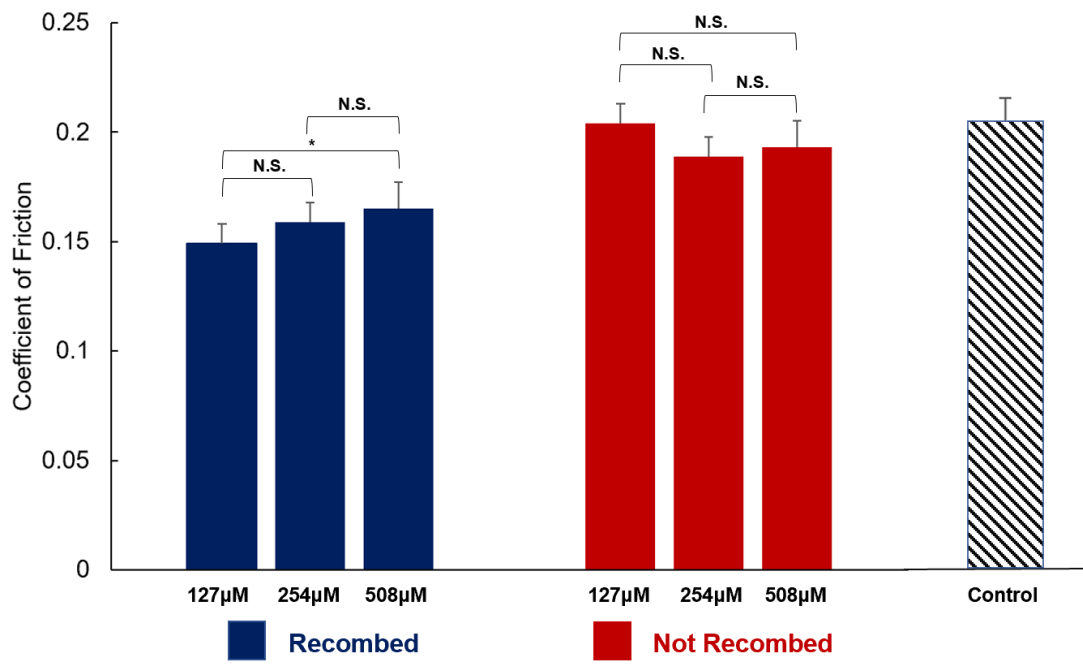
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Figure 5. Particle thickness of 127µM, 254µM and 508µM comparing COF between recombined (blue) and not recombined (red). Error bars indicate standard deviation. ** denotes

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significant differences at $p < 0.001$.



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Figure 6. Particle thickness of 127µM, 254µM and 508µM comparing COF within recombined

166 (blue) and not recombined (red). Error bars indicate standard deviation. * denotes significant
167 differences at $p = 0.01$. N.S. denotes Not Significant at $p < 0.05$.

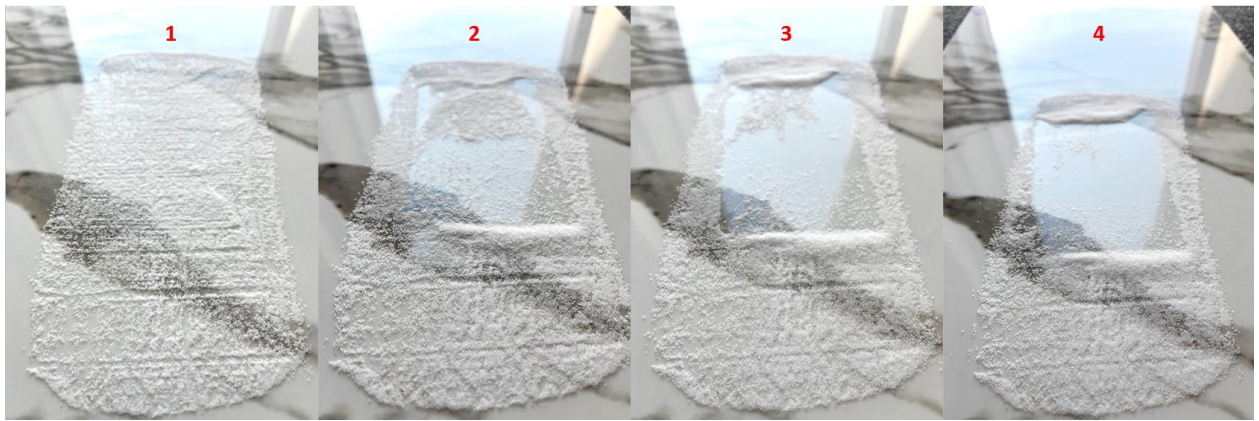
168 Discussion

169 The purpose of this study was to establish a standardized methodological approach to
170 measuring the thickness of particle level and determine if there is an effect of recombining and
171 thickness level of particulate matter on the coefficient of friction. In support of our hypothesis,
172 thinner levels of particulate matter resulted in a lower COF on the tile floor. Furthermore, in
173 support of our hypothesis, particulate matter that was recombined exhibited significantly lower COF
174 compared to particulate matter that was not recombined.

175 This study addressed several methodological gaps from prior research. Previous works, such
176 as those by Li et al. (2014), did not account for the redistribution of particles between tribometer
177 strikes which likely introduced inconsistencies in COF readings. By recombining the particles after
178 each test, this study ensured consistent particle thickness, thereby improving the reliability of the
179 measurements. The significant differences in COF values between recombining and not recombining
180 layers highlight the importance of maintaining consistent particle distribution when evaluating slip
181 resistance.

182 The recombining of dry contaminants is necessary for accurate representation of slip hazards
183 on pedestrian walkways. For each given particle thickness level, the COF was significantly lower
184 in conditions with the recombining compared to the not recombined contaminants. Furthermore, the
185 recombined COF was significantly lower compared to the tile (not contaminated), and the not
186 recombined COF was not significantly different compared to the tile (not contaminated). One
187 possible explanation is that without recombining, the tribometer test foot may clear away most of

188 the contaminant, effectively testing the clean tile rather than the contamination layer (Fig. 7). The
189 test foot essentially strikes the tile directly and pushes the contaminants away from the test foot
190 revealing an almost clean tile for consecutive strikes. In contrast, the recombed material was
191 significantly lower than the control and not recombed conditions as the test foot was striking the
192 dry contaminants each time a slip resistance test was performed, thus result in a lower COF.



193
194 Figure 7. Sequential photographs showing the progressive displacement of dry contaminants
195 after three consecutive tribometer strikes without recombing, demonstrating the loss of uniform
196 particle distribution over repeated trials and the accumulation of particles pushed away from the
197 test foot striking location.

198 The comb-based approach developed in this study offers a novel, accessible, and cost-
199 effective solution for standardizing dry contaminant testing. Using a 3D printer and polylactic acid
200 material, the combs were designed and fabricated at a minimal cost, making this methodology
201 affordable and readily available for widespread use. To ensure precision, the 3D printing process
202 requires approximately 10 hours per comb, with slower speeds improving resolution for the 127
203 μm depth. This approach has the potential to be implemented in various contexts, including
204 academic research, forensic investigations, and industry testing, without requiring substantial
205 financial or technical resources.

206 Despite its contributions, this study is not without limitations. Only one type of particle
207 (iodized salt) and one flooring material (high gloss porcelain tile) were tested. Future research
208 should explore other contaminants (e.g., sawdust, flour, industrial powders) and flooring types
209 (e.g., linoleum, untreated concrete) to broaden the method's applicability and determine whether
210 similar effects are observed. Another limitation arises from the recombining methodology providing
211 consistency, whereas real-world contamination scenarios may involve irregular distribution which
212 could influence slip-resistance outcomes. As this study was designed to be a methodological and
213 proof of concept study, it was not designed to address multiple contaminants and floor types.

214 Practically, these findings have significant implications for slip-resistance testing and floor
215 safety standards. Dry contaminants, such as iodized salt, flour, salt, dust, sawdust, and other
216 particles, are common in both residential and occupational environments. The demonstrated
217 impact of particle thickness on COF highlights the need for safety protocols that account for the
218 presence and distribution of dry contaminants. Future work could expand on these findings by
219 investigating the effects of different particle shapes, material compositions, and rough flooring
220 surfaces to develop a comprehensive understanding of their influence on slip resistance.

221 This study introduces a standardized, reproducible, and cost-effective approach and
222 methodology for standardized dry contaminant slip-resistance testing. The use of 3D-printed
223 combs allows for precise particle thickness control, addressing methodological inconsistencies in
224 prior research. These findings have practical implications for safety testing, forensic
225 investigations, and workplace hazard assessments.

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