

Forecasting Liquefaction Hazard from Seattle Fault Zone Earthquakes: Impacts on a Major Metropolitan Area

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Abstract:

The Seattle Fault Zone (SFZ), a 70-km-long thrust fault system beneath Seattle, Washington, poses a significant seismic hazard to the Puget Sound region due to its proximity to dense urban infrastructure. While other coseismic hazards, such as tsunamis, landslides, and structural damage, have been forecasted for SFZ earthquakes and garnered considerable attention, soil liquefaction—despite its potential for widespread disruption—remains understudied. This study forecasts the spatial distribution of liquefaction and its potential impacts on civil infrastructure from three $M_w7.2$ SFZ earthquake scenarios. Leveraging an ensemble of 18 popular cone-penetration-test based liquefaction models at 268 newly compiled study sites, 14,472 individual high-quality liquefaction predictions are made across the Puget Sound region. Results reveal that severe liquefaction is expected in Seattle and nearby suburbs, particularly within 20 km of the fault along the Interstate-5 corridor, where fill and alluvial soils are prevalent. Comparisons to the 2001 $M_w6.8$ Nisqually earthquake and a potential $M_w9.0$ Cascadia Subduction Zone rupture indicate that SFZ earthquakes are expected to produce more severe liquefaction effects near Seattle due to their closer proximity and greater shaking intensities at short-to-moderate periods. Additionally, liquefaction-induced damage to shallow foundations is predicted to be widespread in Seattle and its suburbs but more limited in areas farther from the fault. These findings provide insights for government agencies and stakeholders to better prepare for future SFZ ruptures.

Keywords: Soil Liquefaction; Seattle Fault Zone; Earthquake Engineering; Liquefaction Hazard; Natural Hazard; Ground Failure

1.0 Introduction and Motivation

The Seattle Fault Zone (SFZ), a 70-km-long thrust fault system, stretches east-west beneath the city of Seattle, Washington, and is considered the most hazardous crustal fault in the U.S. Pacific Northwest due to its proximity to a major urban center (Liberty and Pratt 2008). The SFZ is capable of producing earthquakes in the magnitude range of $M_w7.0$ – 7.5 (e.g., ten Brink et al. 2006; Nelson et al. 2014; Styron and Sherrod 2021) and evidence of surface deformation suggests that moderate-to-large earthquakes ($\sim M_w 5.5$ – 7.5) may occur every few hundred years during active phases lasting approximately 1,000–2,000 years,

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28 followed by quiescent periods lasting several thousand years or more (Nelson et al. 2014). The most recent
29 large rupture, which occurred between 900–930 CE (Bucknam et al. 1992; Atwater, 1999; Sherrod 2001),
30 caused significant geological effects such as liquefaction (Atwater 1999; Atwater personal communication
31 2020; Bourgeois and Johnson 2001; Martin and Bourgeois 2012; Whistler et al. 2002), tsunamis (Atwater
32 1999; Atwater and Moore 1992; Bourgeois and Johnson 2001), and landslides (Jacoby et al. 1992; Karlin
33 et al. 2004; Ludwin et al. 2005; Schuster et al. 1992). Black et al. (2023) further constrained this SFZ rupture
34 to a 6-month period between 923 and 924 CE using dendrochronological dating methods and suggested it
35 may have been a multi-fault $M_w7.8$ rupture involving simultaneous rupture of the SFZ and Saddle Mountain
36 fault.

37 In anticipation of future SFZ earthquakes, several hazards have been forecasted, including tsunamis
38 (Chamberlin and Arcas 2015; Dolcimascolo et al. 2022; Koshimura et al. 2006; Martin 2012; Raulerson
39 2021;), landslides (Allstadt et al. 2013; Grant (2017); Herzig et al. 2024), and shaking-related structural
40 damage (Stewart 2005). These hazards have garnered considerable attention (e.g., Dolcimascolo et al.
41 2022), and decisions on public safety have directly stemmed from them. However, one critical hazard from
42 a SFZ rupture—soil liquefaction—has received comparatively less attention, despite its potential to cause
43 extensive economic and infrastructural damage (e.g., Huang and Yu 2013). Liquefaction, a phenomenon
44 where loose saturated sand-like soils lose strength due to earthquake shaking, has historically caused severe
45 impacts, as exemplified by the Canterbury, New Zealand earthquakes, where liquefaction alone accounted
46 for approximately \$10 billion in damages (Parker and Steenkamp, 2012). In Seattle and the surrounding
47 Puget Sound region, the potential impacts of liquefaction are particularly concerning given the dense urban
48 infrastructure, including buildings, bridges, port structures, roads, levees, and lifelines. For example,
49 Stewart (2005) estimated that a scenario $M_w6.7$ SFZ earthquake could result in 9,700 destroyed buildings,
50 154,500 moderately or severely damaged buildings, 24,200 injuries, and 1,660 fatalities, with liquefaction
51 contributing significantly to these impacts. While these estimates rely on numerous simplifying
52 assumptions and warrant further investigation, they underscore the potentially staggering impact of
53 liquefaction from a SFZ rupture.

54 Instances of liquefaction have been documented in the Puget Sound region during the region's recent
55 large historical earthquakes, such as the 1949 $M_w7.1$ Olympia earthquake and the 1965 $M_w6.5$ Seattle-
56 Tacoma earthquake (Chleborad and Schuster 1990). While these events caused only moderate damage in
57 Seattle due to relatively low peak ground accelerations (*PGAs*) of approximately 0.10 g (Rogers et al. 1998),
58 they serve as a reminder of the hazard's potential. Grant (1986) estimated that 25–50% of the total damage
59 from these earthquakes could be attributed to ground failures such as liquefaction. More recently, the 2001
60 $M_w6.8$ Nisqually earthquake also damaged infrastructure throughout the Puget Sound region causing \$2 to
61 4 billion in damage (Creager et al. 2001). Despite these past earthquakes, the damage potential in Seattle is

62 expected to be far greater in a large SFZ event compared to any other seismic source in the region due to
63 the shallow depth of the fault and its close proximity to the city, leading to significantly higher shaking
64 intensities, particularly for short-to-moderate periods.

65 Despite its importance, the only prior attempt to forecast the spatial distribution of liquefaction in an
66 SFZ rupture is Stewart's (2005) study, which employed the HAZUS geospatial modeling approach (e.g.,
67 FEMA 2019). This method assigns broad hazard classifications (e.g., "low" to "high") to geologic units
68 based on several simplifying assumptions. While useful for providing a first-order approximation,
69 geospatial models like HAZUS, which infer soil traits from geologic maps, are inherently less reliable than
70 mechanistic liquefaction models that use detailed below ground geotechnical data. As a result, neither the
71 expected spatial distribution of liquefaction in a large SFZ event nor its damage potential for infrastructure
72 is currently understood with confidence.

73 Mechanistic models, first developed in the 1970s (e.g., Seed and Idriss, 1971), have significantly
74 advanced the prediction of liquefaction occurrence and damage potential using geotechnical test data. These
75 state-of-practice models, refined over decades with expanded datasets (e.g., Geyin et al. 2021), achieve
76 global prediction efficiencies of ~75–85% (e.g., Geyin and Maurer 2020a). For instance, during the
77 Nisqually earthquake, a popular ensemble of these models demonstrated ~90% efficiency in predicting
78 liquefaction occurrence (Rasanen et al., 2023a). Despite their proven reliability, no study has applied these
79 mechanistic liquefaction models to predict the spatial distribution and damage potential of liquefaction in
80 a large SFZ earthquake.

81 Accordingly, this study aims to fill this critical knowledge gap by forecasting the spatial distribution of
82 liquefaction and its potential impacts on civil infrastructure during a large SFZ event using state-of-practice
83 liquefaction models. This study first introduces the expected ground motions from three M_w 7.2 SFZ
84 earthquake scenarios and the geotechnical data used. It then presents the liquefaction modeling
85 methodology followed by a discussion of the results with comparisons to past earthquakes. Lastly, the
86 conclusions are presented. This research provides valuable insights to aid government agencies and
87 stakeholders in preparing for and mitigating the risk of liquefaction posed by future SFZ earthquakes.

88 **2.0 Data and Methodology**

89 **2.1 Seattle Fault Zone Scenarios**

90 The Building Seismic Safety Council 2014 (BSSC2014) Event Set (Thompson et al. 2016) includes rupture
91 scenarios of characteristics earthquakes on all known active faults in the United States as included in the
92 2014 version of the USGS national seismic hazard maps (Petersen et al. 2014). The ground motion intensity
93 measures (e.g., *PGA*) in this catalog were computed using a weighted combination of ground motion models
94 for reference rock conditions that are consistent with the 2014 USGS national seismic hazard maps

95 (Petersen et al. 2014). To account for local soil conditions, the BSSC2014 scenarios used the time averaged
96 shear wave velocity over the top 30 meters (V_{s30}) to compute empirical site amplification factors (V_{s30} -based
97 site amplification). Each of the ground motions models used its own site response model (e.g., Chiou and
98 Youngs 2014) or one developed for particular ground motion models (e.g., Seyhan and Stewart 2014). The
99 input V_{s30} values are a combination of a global model estimated from topographic slope (Wald and Allen
100 2007) and regional models that are available at the USGS Global V_{s30} GitHub repository (Worden and
101 Heath, 2019). As part of the BSSC2014 scenario catalog, three SFZ zone earthquake scenarios were
102 modelled—the northern, middle, and southern scenarios. Each of the three SFZ scenarios were modelled
103 as M_w 7.2 ruptures along a thrust fault at 9 km depth, but with varying locations and lengths (Petersen et al.
104 2008). Therefore, the shaking produced between the scenarios differs, especially in the near-field. The
105 ground motion estimates for each of the scenarios include site-adjusted mean and standard deviation values
106 for multiple intensity measures (e.g., PGA). In addition to ground motions estimates derived from ground
107 motion models, physics-based ground motion simulations have more recently been developed for the SFZ.
108 Stone et al. (2022) produced 20 physics-based simulations of M_w 6.5-7.0 SFZ earthquakes using a variety
109 of slip distributions and hypocenter locations. While the Stone et al. (2022) simulations potentially offer
110 improved estimates of ground shaking at many frequencies, there are drawbacks for using them to predict
111 regional liquefaction. First, the spatial extent of the Stone et al. (2022) simulations is limited to ~40 km
112 from Seattle and thus does not cover the extent at which liquefaction can occur during a SFZ earthquake.
113 Second, the SFZ simulations are modeled up to a frequency of 3 Hz, whereas PGA is the most efficient,
114 sufficient, and commonly used intensity measure for predicting liquefaction (e.g., all state-of-art
115 liquefaction response models use PGA) (Sideras, 2019). Therefore, to predict liquefaction across the region
116 with the Stone et al. (2022) simulations, modification for use of high frequencies would be required in
117 addition to a methodology to ensemble them with a GMM so they can be extended to sites across the region,
118 both of which would add uncertainty to the predicted ground shaking. Therefore, while the Stone et al.
119 (2022) simulations are an excellent source for many studies (e.g., Herzig et al. 2024), the SFZ BSSC2014
120 scenarios are used in this study to predict regional liquefaction impacts. Mean site-adjusted $PGAs$ are shown
121 for the three SFZ scenarios in Figure 1 along with 268 locations of subsurface geotechnical data as discussed
122 in the following section. These mean PGA estimates, along with the corresponding standard deviation, are
123 used to compute a probability density function (PDF) of PGA for use in liquefaction forecasts.

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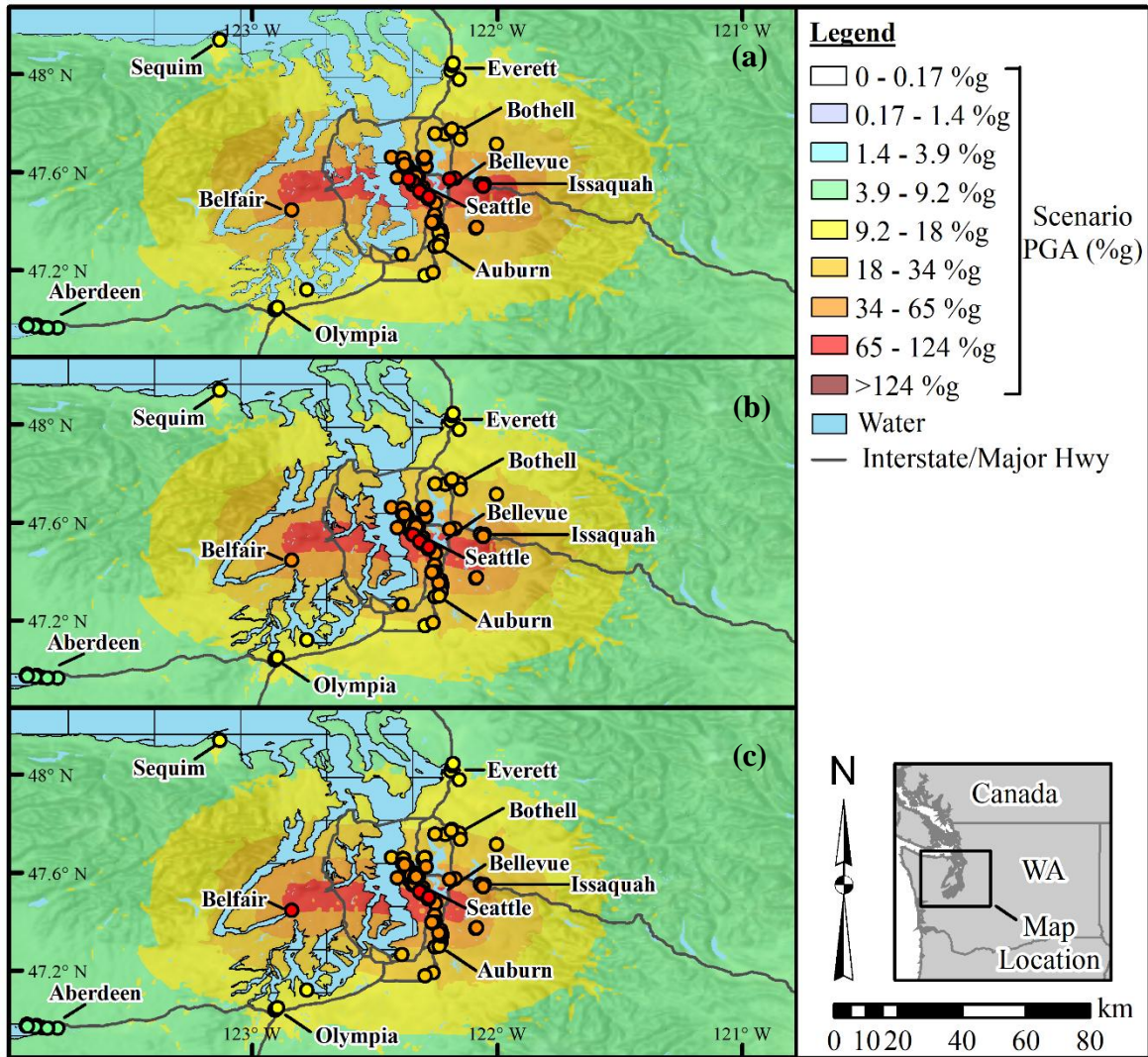


Fig. 1 Seattle fault shakemap of mapped *PGA* (%g) for (a) northern; (b) middle; and (c) southern scenarios with the locations of 268 study sites marked with circles. *PGA* = peak ground acceleration.

125 2.2 Subsurface Data and Methodology

126 To predict liquefaction response at 268 locations, a newly compiled dataset of CPT measurements and other
 127 geotechnical data was assembled from various sources, including Jeschke et al. (2019), Chin and Evans
 128 (2021), the Washington State Dept. of Transportation (WSDOT 2021), and Grant et al. (2024). The selected
 129 study sites were chosen based on SFZ scenarios predicting a *PGA* of at least 0.08 g at each site, which
 130 represents the minimum estimated *PGA* required to trigger liquefaction in even the most susceptible soils
 131 (de Magistris 2013). This dataset is made available in Rasanen et al. (2024; 2025) to support future research.
 132 Given the importance of saturation, groundwater depths were collected from the geotechnical reports that
 133 documented CPTs in addition to supplemental information from nearby borings, well logs, and test pits. In
 134 most cases, multiple groundwater depth measurements were available near each CPT location due to the

135 region’s extensive subsurface exploration history. The locations of the 268 study sites are shown in Figure
136 1. They are spatially distributed but concentrated along the Interstate-5 (I-5) corridor from Olympia, WA
137 to Everett, WA, including Seattle and many of its suburbs, and in coastal towns (e.g., Aberdeen, WA and
138 Sequim, WA).

139 **2.3 Liquefaction Modeling**

140 Liquefaction triggering was predicted over the depths of each CPT profile using six established CPT-based
141 methods: Robertson and Wride (1998), Architectural Institute of Japan (2001), Moss et al. (2006), Idriss
142 and Boulanger (2008), Boulanger and Idriss (2016), and Green et al. (2019). Following findings from Geyin
143 and Maurer (2021b) and Yost et al. (2021), no inversion filter was applied to account for thin-layer effects
144 in the CPT data. Liquefaction susceptibility was assessed using soil behavior type index (I_c) (Robertson and
145 Wride, 1998). To address the uncertain relationship between I_c and susceptibility, the Maurer et al. (2019)
146 model was employed to estimate the probability of susceptibility, as defined by Boulanger and Idriss (2006),
147 based on the measured I_c values. Since liquefaction occurring at depth may have minimal impact or fail to
148 manifest at the ground surface, the results of the triggering analysis were used as inputs to three additional
149 models to predict surficial manifestations of liquefaction (i.e., “ground failure”). These models—developed
150 by Iwasaki et al. (1978), van Ballegooy et al. (2014), and Maurer et al. (2015)—do not explicitly predict
151 infrastructure damage, but offer practical proxies of damage potential. Because more severe surface
152 manifestations of liquefaction correlate with a higher likelihood of damage to near-surface infrastructure
153 such as buildings, bridges, and roads, these models can provide insight into the potential severity of impacts.
154 The combined use of six triggering models and three manifestation models resulted in 18 model
155 combinations. Probabilistic predictions of surficial liquefaction manifestations were made for these 18
156 models using fragility functions developed by Geyin and Maurer (2021a). With this methodology, the
157 probability of manifestation was computed using the total probability theorem as:

$$158 \quad P(\text{Manifestation}) = \int_{PGA} \int_{I_c} P(\text{Manifestation}|PGA, I_c) f(I_c) f(PGA) \cdot dI_c \cdot dPGA \quad (1)$$

159 Where $f(I_c)$ is the probability density function of the I_c threshold for discriminating susceptibility (Maurer
160 et al., 2019); $f(PGA)$ is the probability density function (PDF) computed from a weighted combination of
161 ground motion models (GMMs) considering site response (Thompson et al. 2016); and
162 $P(\text{Manifestation}|PGA, I_c)$ is the probability of surficial manifestation, which is conditioned on PGA and
163 the susceptibility threshold I_c , among other inputs, and which is computed via the fragility functions of
164 Geyin and Maurer (2021a). Rasanen et al. (2023a) evaluated the performance of these 18 models using 24
165 case histories from the 2001 Nisqually, WA, earthquake. While the predictive efficiencies of the models
166 varied, the differences were generally not statistically significant when accounting for finite-sample

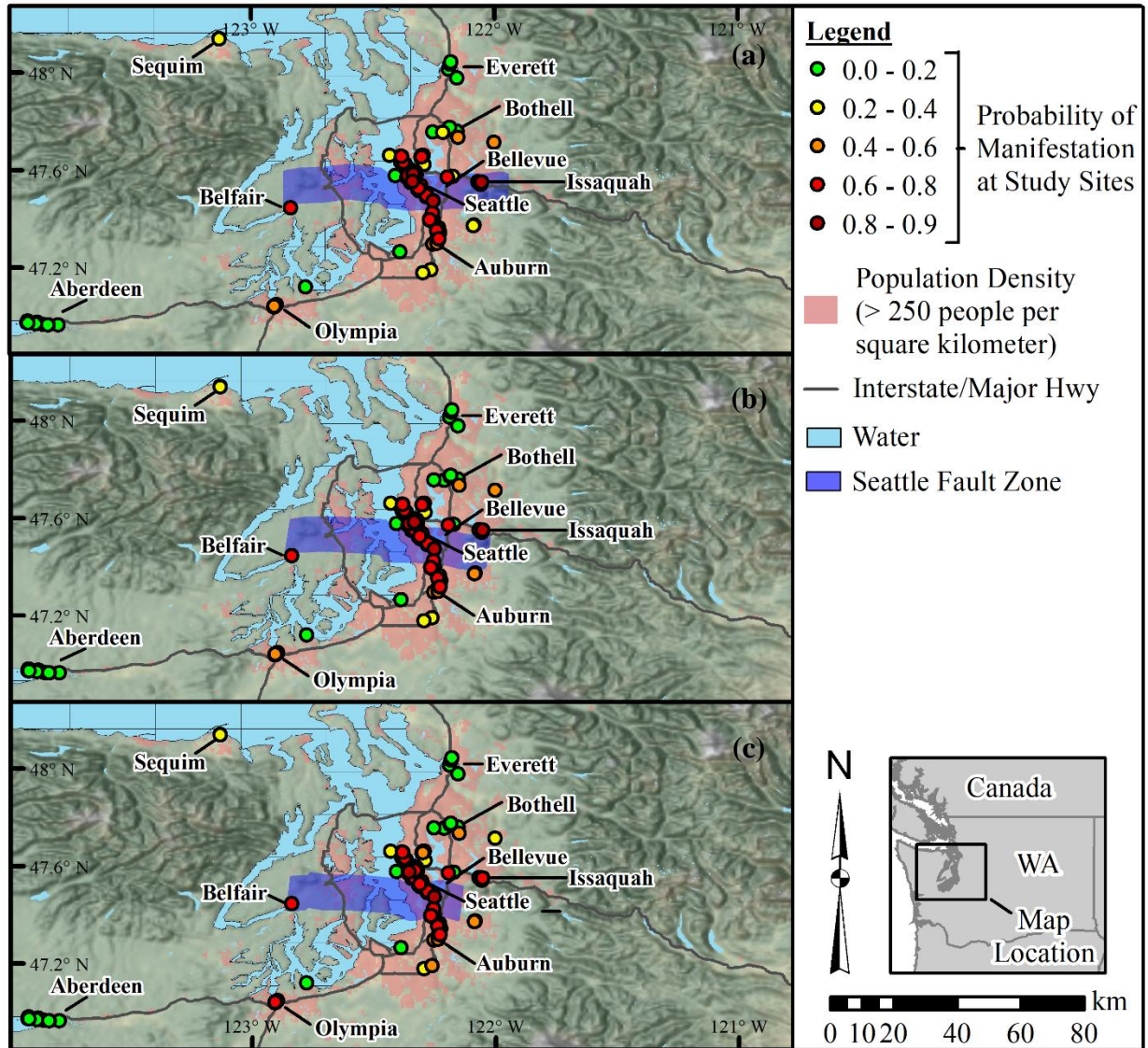
167 uncertainty. Therefore, in this study, predictions from all 18 models were combined using an ensemble
168 approach with equal weighting.

169 **3. Results and Discussion**

170 **3.1 Liquefaction Predictions**

171 Using the data and methodology described above, the probability of surficial liquefaction manifestation
172 was computed at 268 study sites for each of the 18 liquefaction models and the three SFZ ground-motion
173 scenarios, resulting in 14,472 individual high-quality liquefaction predictions. The ensembled liquefaction
174 probabilities, shown in Figure 2 for each SFZ scenario, indicate that the highest probabilities occur along
175 the I-5 corridor near Seattle, WA. Given the sites available for study, probabilities exceeding 60% are in
176 general predicted as far south as 30 km from Seattle, as far north as 20 km from Seattle, as far east as
177 Issaquah, WA 25 km away from Seattle, and as far west as Belfair, WA 40 km away from Seattle. Also of
178 note, are probabilities exceeding 60% in Olympia, WA (75 km from Seattle) for the southern SFZ scenario,
179 and probabilities exceeding 20% as far Northwest as Sequim, WA for all scenarios. These predictions
180 indicate that liquefaction could be widespread throughout the Puget Sound region, particularly near Seattle,
181 posing substantial risks to densely populated areas, critical transportation networks, and infrastructure.
182 Further away from the SFZ, the probabilities in Aberdeen, WA generally range from 1% to 5% and
183 occasionally exceed 10% for all scenarios, while the probabilities in Everett, WA generally range from 10%
184 to 20% where the northern scenario generally predicts ~2% higher probability on average. While the
185 predicted probabilities are low in Aberdeen and Everett from a SFZ earthquake, other earthquakes such as
186 a Cascadia Subduction Zone rupture (Rasanen et al. 2025) for Aberdeen, or a Whidbey Island crustal fault
187 rupture for Everett, would almost certainly be more severe in those locations. Furthermore, this should not
188 be taken to mean that liquefaction can only occur at the study sites investigated in this article. Rather, these
189 are the locations where high-quality subsurface data is available to make predictions. It must be emphasized
190 that while these predictions may generally extrapolate to areas surrounding each test site, liquefaction is a
191 localized phenomenon and therefore nothing can be known with certainty at unsampled locations.

192



193 **Fig. 2** Probability of liquefaction surface manifestation at 268 study sites considering the (a) northern; (b) middle; and (c) southern Seattle fault ground motion scenarios.

194 Due to the dense population and strong ground motions expected in the near-field for each scenario,
 195 Figure 3 provides a higher-resolution view of the predicted probability of liquefaction manifestation at
 196 study sites within a section of Seattle. Figure 3 provides results from the northern and southern SFZ
 197 scenarios, which among the three scenarios produce motions that differ the most. In this regard, the
 198 probability of liquefaction manifestations for the middle scenario are mapped in supplemental Figure S.4.
 199 Comparing liquefaction response between SFZ scenarios, the northern scenario predicts probabilities to be
 200 5% larger on average than the southern scenario. This is the result of the northern SFZ scenario traversing
 201 beneath more of the Seattle study sites (rather than south of them) leading to a larger *PGA* prediction. In
 202 that regard, study sites in the near-field have larger probability differences between SFZ scenarios compared

203 to study sites further from the SFZ due to the larger differences in *PGA* in the near field. As an example,
204 the probabilities in Seattle, Auburn, and Issaquah differ by ~5% between the northern and southern
205 scenarios, but differ by ~2% in Everett and Olympia and trend to negligible differences further away in
206 locations like Aberdeen. While perceptible differences in predictions of liquefaction exist between the SFZ
207 scenarios, all scenarios predict significant liquefaction in Seattle with the average across the three scenarios
208 exceeding 60% at 92 of the 140 study sites. The areas expected to be impacted most are the Greater
209 Duwamish, Interbay, and University districts where a majority of the test data is located (see Figure 3). Of
210 these districts, the Duwamish is expected to be most severely impacted by liquefaction with 70% of study
211 sites having a probability > 60%, followed by Interbay (62%) and the University district (22%). Notably,
212 these districts all have areas of extensive artificial fill and experienced liquefaction in the 1949, 1965, and/or
213 2001 earthquakes (e.g., Chleborad and Schuster 1990; Bray et al. 2001). To provide context for the
214 computed probabilities, predictions of liquefaction for a SFZ earthquake are compared to those made for
215 the 2001 Nisqually earthquake, which benefited from dense ground motion recordings and where observed
216 liquefaction damage provides a benchmark for evaluating the relative severity of future events. Using the
217 same modeling approach for the Nisqually event (Rasanen et al., 2023a), liquefaction probabilities in the
218 Duwamish district for an SFZ scenario are approximately double those of the Nisqually event, while in
219 Interbay and the University districts, probabilities are as much as 10 times higher. Therefore, the frequency
220 and severity of liquefaction in the Duwamish district may be twice that experienced in 2001, where
221 structures in the area were extensively damaged by liquefaction-induced foundation failure, with some
222 foundations settling by as much as 4 feet. In total, 26 buildings in Seattle were red-tagged and 161 others
223 yellow-tagged, the majority of which in the Duwamish district (Creager et al. 2001). For the Interbay and
224 University districts, direct comparisons to the Nisqually event are more challenging due to minimal
225 observed liquefaction and damage during the 2001 earthquake, a result of the northward attenuation of
226 ground motions in that event. Nevertheless, given the proximity of these districts to the SFZ, significantly
227 larger ground motions are expected compared to Nisqually, and the resulting liquefaction hazards would
228 likely lead to far greater damage in these areas.

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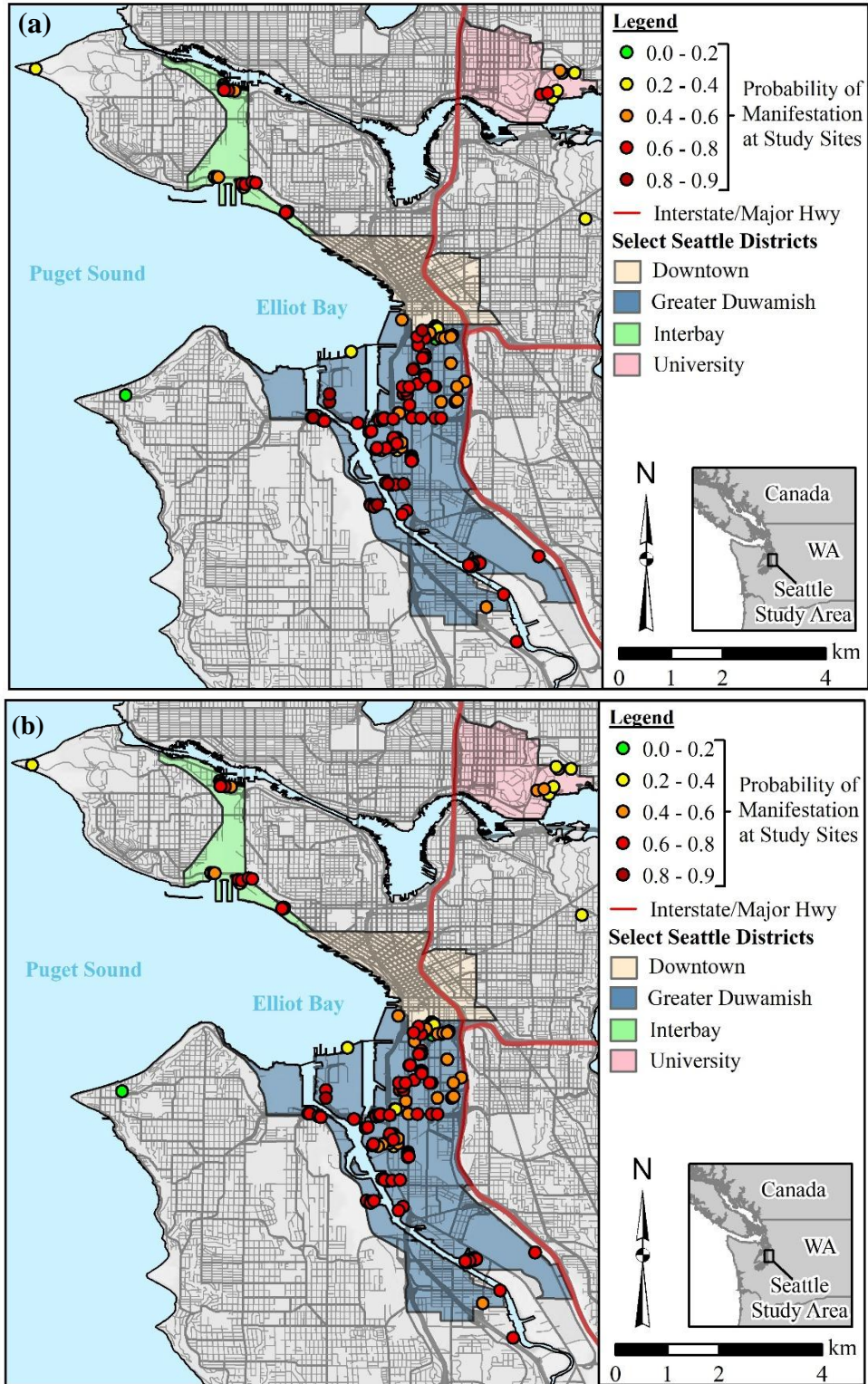


Fig. 3 Probability of liquefaction surface manifestation at study sites in Seattle, WA, considering the (a) northern; and (b) southern Seattle fault ground motion scenarios.

230 It should be noted in the context of Figures 2 and 3 that predictions cannot be extrapolated well beyond
231 the study sites. In the University district, for instance, study sites near the University of Washington’s
232 athletic facilities are on land that was formerly beneath the surface of Lake Washington before its lowering
233 around 1915, and where artificial fill is prevalent. In contrast, most of the University campus just to the
234 west lies at higher elevations on glacial till, where the liquefaction hazard is expected to be very low. Similar
235 statements could be made for the Interbay and Duwamish districts that also have reclaimed land.
236 Importantly, this does not imply that liquefaction hazards are limited to these areas of Seattle. Artificial fill
237 is widespread across the city, and as shown by historical and paleoliquefaction observations in the region
238 (e.g., Rasanen et al. 2021), in addition to global earthquakes occurring each year, alluvium and other natural
239 soil deposits can be equally susceptible to liquefaction. Furthermore, the predictions shown in Figure 3 are
240 not representative of the entire city. Study sites are typically located where liquefiable soils are more likely
241 to be found—such as areas with artificial fill or alluvium—rather than in locations with more resistant
242 ground, like glacial till. Similar patterns can be observed in other municipalities, as CPTs are generally
243 performed in soils that are sufficiently penetrable.

244 **3.2 Comparisons of Seattle Fault Zone to M9 Cascadia Subduction Zone liquefaction**

245 To provide additional details for towns outside Seattle, but still impacted by a SFZ rupture, their
246 liquefaction predictions are discussed in more detail and then compared to liquefaction predictions from a
247 Cascadia Subduction Zone (CSZ) rupture. Rasanen et al. (2025) predicted the regional probability of
248 liquefaction manifestation from 30 M_w 9.0 CSZ simulations. While there is no infrastructure damage to
249 compare to like there is for the 2001 Nisqually earthquake, general comparisons between SFZ and CSZ
250 predictions of liquefaction can be made. To that end, the SFZ predictions are compared to the median
251 probabilities of the 30 M_w 9.0 CSZ events.

252 ***Aberdeen, Washington:*** Probabilities in Aberdeen, WA for all scenarios generally range from 1% to 5%
253 and occasionally exceed 10%. In general, the Southern Seattle fault scenario provides the highest
254 predictions, although the differences are negligible between scenarios (~1%). The low probabilities in
255 Aberdeen compared to other locations discussed are mainly due to Aberdeen’s distance from the SFZ. The
256 western extents of the three rupture scenarios are approximately 90 km from Aberdeen, allowing more
257 distance for ground motions to attenuate. Therefore, the strength of ground shaking is much lower in
258 Aberdeen (~0.08 g) compared to other near-fault locations like Seattle (~0.5-0.8 g) for the SFZ scenarios.
259 Comparing to the expected liquefaction impacts from a CSZ rupture, Rasanen et al. (2025) predicted a
260 median liquefaction response that ranged from 30-75% at the study sites in Aberdeen. Therefore, while the
261 probability of liquefaction is low in Aberdeen for a SFZ rupture, other seismic sources such as the CSZ are
262 likely to produce liquefaction.

263 **Everett, Washington:** Everett, WA is approximately 50 km north of the SFZ along I-5. The probabilities in
264 Everett, WA generally range from 10 to 20%, where the north scenario generally predicts ~2% higher
265 probability on average. Comparing with the expected liquefaction impacts from a CSZ rupture, Rasanen et
266 al. (2025) found median liquefaction probabilities ranged from 20% to 47%. Therefore, although Everett is
267 much closer to the SFZ than to the CSZ, the greater magnitude and longer shaking duration of a CSZ rupture
268 results in higher probabilities of liquefaction manifestation in Everett.

269 **Auburn, Washington:** Auburn, WA is approximately 15 to 25 km south of the SFZ. The probabilities in
270 Auburn generally range from 50% to 70%. The southern Seattle fault scenario provides the highest
271 predictions for all sites in Auburn with probabilities 5% larger than the northern scenario on average. Thus,
272 while the ground motions may appear similar in Figure 1 between scenarios, there are perceptible
273 differences in liquefaction response owing to the differences in the ground motions at the site. Interestingly,
274 CSZ median liquefaction probabilities are generally within ~1% to 2% of the middle Seattle fault scenario
275 (i.e., between the southern and northern SF scenario predictions). While the median expected ground
276 motions for a CSZ rupture in Auburn, WA (~0.17 g) are anticipated to be less than the *PGA* for the SFZ
277 scenarios (~0.27 g to 0.31 g), the larger magnitude Cascadia rupture (M_w 9.0) would have a longer duration
278 of shaking than a M_w 7.2 SFZ rupture, thus leading to more cycles of loading and ultimately leading to
279 similar liquefaction predictions in Auburn.

280 **Bothell, Washington:** Bothell, WA is approximately 20 km north of the SFZ. A majority of the SFZ
281 liquefaction probabilities in Bothell are less than 5%, however, one study site has a probability over 50%.
282 The *PGAs* at the study sites ~0.17 g to 0.25 g are certainly capable of triggering liquefaction, however, the
283 soils at a majority of the study sites in Bothell are either not sufficiently loose, saturated, or cohesionless to
284 liquefy, and/or the strata predicted to liquefy are interpreted to not be sufficiently thick or shallow to
285 produce surface manifestations. In general, CSZ predictions are 0% to 20%, however, one study site
286 exceeds 60% while a few others exceed 40%. Thus, the median probability of liquefaction predictions for
287 a CSZ rupture are slightly larger than those of the SFZ scenarios in Bothell.

288 **Issaquah, Washington:** Issaquah, WA is approximately 20 km east of Seattle near the eastern extent of the
289 SFZ. The liquefaction probabilities in Issaquah, WA generally range from 54% to 81%. The median CSZ
290 liquefaction probabilities range from 33% to 72%, which are lower than the SFZ predictions although some
291 locations still have relatively high probability.

292 **Belfair, Washington:** Belfair, WA is at the southwestern extent of the SFZ for all three scenarios near the
293 terminus of the Hood Canal (fjord). The probability of manifestation near Belfair, WA was computed at a
294 single study site and ranged from 69% for the northern scenario to 72% for the southern scenario. The
295 median liquefaction prediction from a CSZ rupture was computed to be 75%, similar to the SFZ predictions.

296 While the SFZ scenario *PGAs* are 0.1 g to 0.2 g larger than the CSZ *PGA*, the increased duration of the
297 CSZ earthquake causes the slightly larger liquefaction probability for this site.

298 ***Olympia, Washington:*** Olympia, WA is approximately 45 km south of the western end of the SFZ. The
299 probabilities in Olympia, WA generally range from 15% to 60%. Compared to the median expected
300 liquefaction impacts from a CSZ rupture, Rasanen et al. (2025) computed median liquefaction probabilities
301 ranging from 40% to 90%, indicating liquefaction from a CSZ rupture is likely to be more prevalent
302 compared to a SFZ rupture.

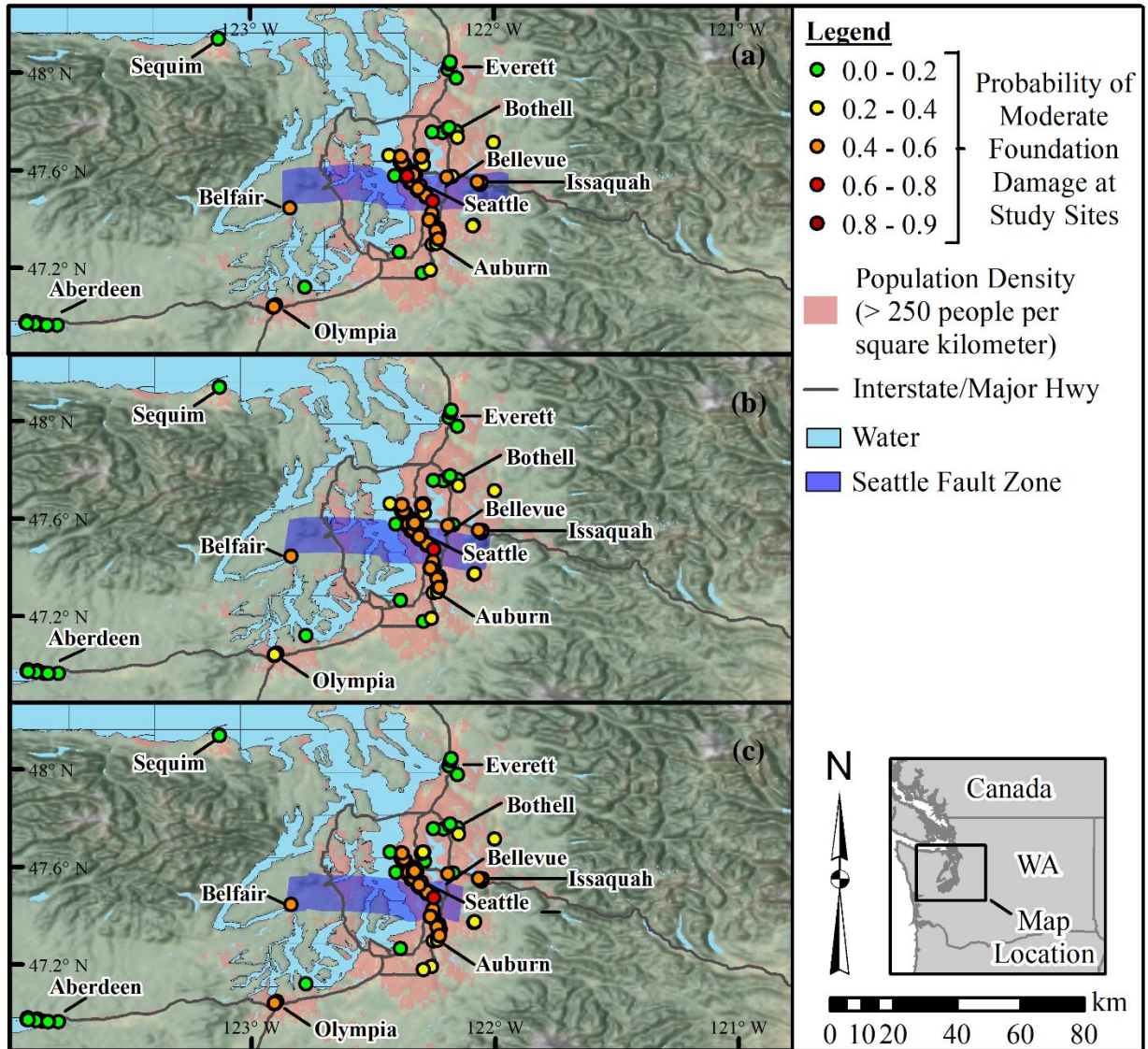
303 ***Seattle, Washington:*** All three SFZ scenarios traverse through the southern portion of Seattle and produce
304 *PGA*'s generally ranging from ~0.5 g to 0.8 g in Seattle. Liquefaction probabilities over the portion of
305 Seattle shown in Figure 3 are 62% on average, with 66% of sites having a probability greater than 60%.
306 The northern scenario has a 5% larger liquefaction probability than the southern scenario on average. The
307 median liquefaction probability for the 30 M_w 9.0 CSZ simulations is on average 41% for the study sites
308 within the extent shown in Figure 3. For these CSZ predictions, only 23% of study sites have a probability
309 >60% given the smaller *PGAs* for the median CSZ rupture in general ranging from 0.10 g to 0.28 g.
310 Therefore, while a CSZ earthquake is capable of being a M_w 9.0, a M_w 7.2 SFZ earthquake is anticipated to
311 cause liquefaction impacts that would be far worse in Seattle compared to a CSZ earthquake due to Seattle
312 residing so close to the SFZ and thus leading to high frequency ground motions 3-5 times larger than the
313 high frequency motions from a CSZ earthquake. This does not mean all earthquake impacts in Seattle would
314 be more severe for a SFZ rupture than a CSZ rupture. Surely, long period shaking and thus tall structures
315 are more likely to be damaged from a CSZ earthquake given the low frequency motions generated by M_w 9.0
316 subduction zone events. However, high frequency motions (e.g., *PGA*), which are best for predicting
317 liquefaction (Sideras, 2019), are anticipated to be far more severe during a SFZ earthquake than the median
318 expected liquefaction response of a CSZ earthquake. Even for the strongest expected shaking from a CSZ
319 earthquake, which predicts 43% of study sites with a liquefaction probability exceeding 60% (Rasanen et
320 al. 2025), the predicted impact remains substantially lower than that of the SFZ scenarios, where 66% of
321 study sites shown in Figure 3 exceed the same liquefaction probability threshold.

322 In general, the liquefaction damage from a SFZ earthquake is anticipated to be worse than the median
323 predictions from a CSZ earthquake in Seattle and along the I-5 corridor as far south as Auburn, WA to as
324 far north as Bothell, WA. SFZ liquefaction predictions are expected to be worse east of Seattle as far as
325 Issaquah, WA. Similar comparisons cannot be made west of I-5 due to the lack of high-quality data to
326 predict liquefaction. One study site at the western extent of the SFZ near Belfair, WA had similar
327 predictions between the SFZ scenarios and the median expected liquefaction response from a CSZ
328 earthquake.

329 The higher predictions of liquefaction from a SFZ earthquake in the Seattle area may be preliminarily
330 corroborated with paleoliquefaction evidence. Interestingly, at the time of writing this article, no
331 liquefaction has been tied to the 1700 CSZ earthquake in the Puget Sound region, let alone any Cascadia
332 Subduction Zone earthquake (Rasanen et al. 2023b; 2025), despite extensive searches (e.g., Atwater 1999;
333 Bourgeois and Johnson 2001; Clague 2002; Clague et al. 1992, Clague et al. 1997, Davis 2018, Martin and
334 Bourgeois 2012, Obermeier 1995; Rasanen et al. 2021). At the same time, liquefaction features constrained
335 to about the time of the 923-924 CE SFZ earthquake have been found at several sites (Atwater 1999;
336 Bourgeois and Johnson 2001; Whistler et al. 2002; Martin and Bourgeois 2012; Atwater personal
337 communication 2020), including some liquefaction features (e.g., Bourgeois and Johnson 2001) extending
338 up to a tsunami deposit tied to the 923-924 AD SFZ earthquake. This disparity between paleoliquefaction
339 evidence for a SFZ versus CSZ earthquake suggests the SFZ poses a greater liquefaction hazard in Seattle
340 and potentially other areas of the surrounding Puget Sound region.

341 **3.3 Probability of Liquefaction-Induced Foundation Damage**

342 The probabilities mapped in Figures 2 and 3 are those of surficial manifestations in the free field (i.e.,
343 liquefaction ejecta and/or ground cracking and deformation coinciding with potentially damaging
344 instability). These manifestations strongly correlate with damage, particularly to shallow foundations,
345 buried lifelines, pavements, and other near-surface infrastructure. However, liquefaction can potentially
346 cause damage without otherwise expressing at the surface or can potentially express at the surface without
347 causing damage. Asset-specific studies are therefore needed to predict the consequences of liquefaction
348 more confidently. To that end, the 2010-2011 Canterbury, New Zealand, earthquakes resulted in
349 unprecedented liquefaction case-history data (e.g., Geyin et al., 2021), including foundation damage
350 surveys. To provisionally go beyond free-field manifestations and speculate on impacts, the foundation-
351 damage models of Geyin et al. (2020b), which were trained using building performance data from
352 Canterbury, were applied to the 268 study sites. These models are conditioned on the manifestation models
353 adopted herein and are specific to 1-2 family residential structures on shallow foundations. The median
354 probability of exceeding “moderate” foundation damage is mapped in Figure 4 for all three scenarios and
355 in Figure 5 (Seattle extent) for the northern and southern SFZ scenarios. In this regard, the middle scenarios
356 predictions fall between the north and south predictions and can be found mapped in supplemental Figure
357 S.8. “Moderate” damage is defined as differential settlement more than 2 cm or global settlement exceeding
358 5 cm, but also includes five other modes of foundation deformation.



359

Fig. 4 Probability of moderate or greater foundation damage from liquefaction at 268 study sites considering the (a) northern; (b) middle; and (c) southern Seattle fault ground motion scenarios.

360

The median probability of such damage exceeds 40% at 69% of the study sites in Seattle, 88% of the sites in Auburn, 63% of the sites in Issaquah, and 15% of the sites in Olympia. As with the probabilities of free field manifestations, those of foundation damage also vary between the three SFZ scenarios by up to ~5%. Based on these preliminary analyses, damage to shallow foundations in Seattle and the surrounding suburbs like Auburn and Issaquah are likely to be relatively common for all scenarios whereas damage in locations like Olympia would likely be more sporadic.

366

367

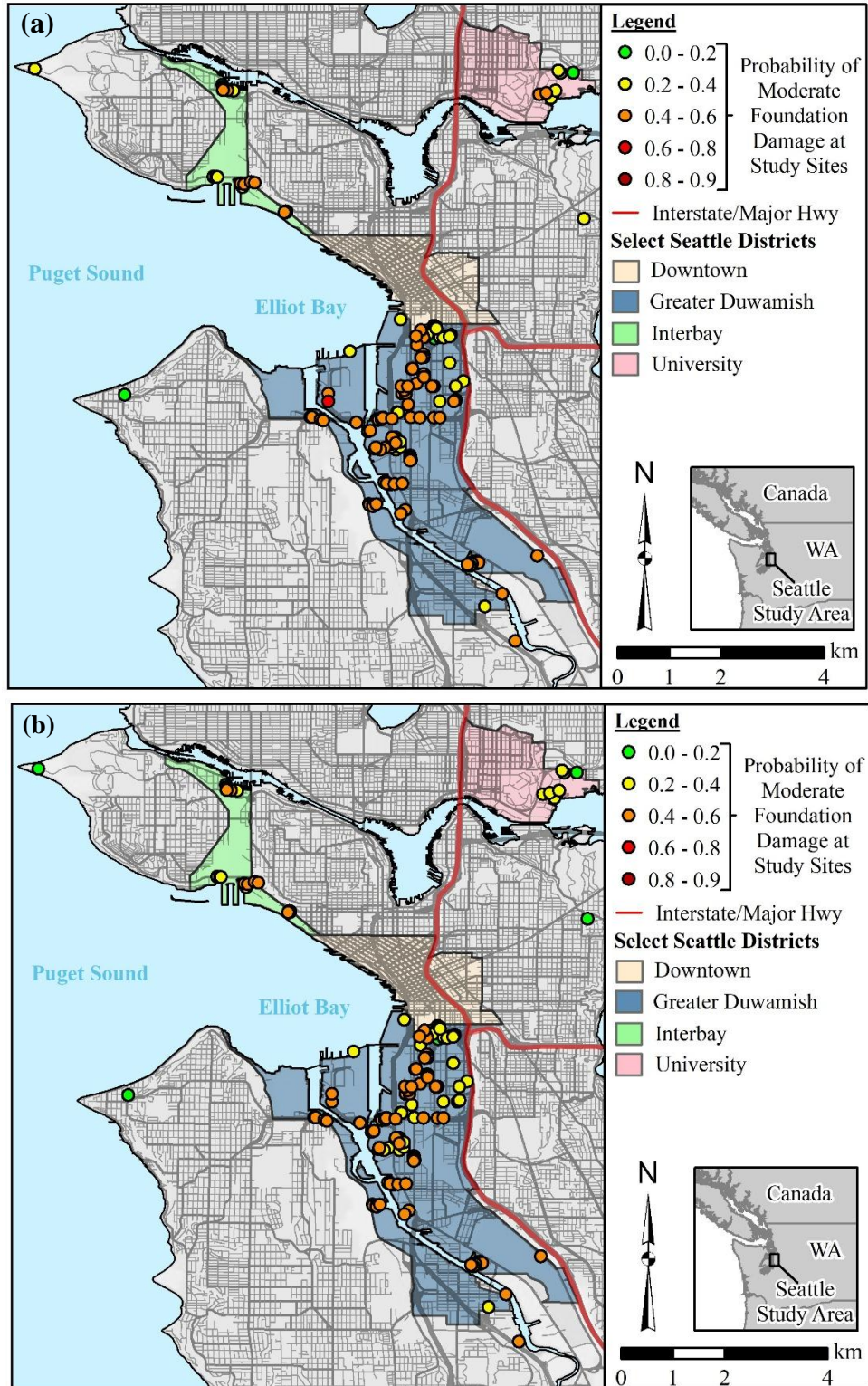


Fig. 5 Probability of moderate or greater foundation damage from liquefaction at 140 study sites in Seattle, WA, considering the (a) northern; and (b) southern SFZ ground motion scenarios.

368 These predictions do not account for potential, additional damage from: (i) lateral spreading, a
369 particularly destructive effect of liquefaction influenced by local terrain; (ii) cyclic softening, which can
370 induce permanent deformation in sensitive fine-grained materials; or (iii) seismic compression, which is
371 the accrual of volumetric strains in dry or partially saturated soils that can lead to ground settlement during
372 earthquake shaking, even at sites where the water table is too deep for damaging liquefaction. It is also
373 important to recognize that: (i) shallow foundations supporting residential structures may not be present at
374 the study sites, meaning these predictions are primarily illustrative; and (ii) many modern infrastructure
375 assets (e.g., commercial, industrial, and large residential buildings) are constructed in compliance with
376 building codes that mandate mitigation of liquefaction hazards, whether through ground improvement or
377 more robust foundation systems. In contrast, older structures and other assets—such as roads, utilities, and
378 residential homes—are less likely to have been designed with liquefaction considerations in mind. For
379 example, single-family and duplex homes fall under the jurisdiction of the International Residential Code
380 (e.g., IRC, 2021), which does not address liquefaction hazards, leaving mitigation up to individual
381 homeowners and local officials. Given this regulatory gap, the low rate of earthquake insurance coverage
382 in Washington—11.3% of residential homeowners are insured (Doughton and Gilbert 2018)—and the
383 predictions mapped in Figures 4 and 5, liquefaction could pose a serious economic risk both to individual
384 owners and to society at large. Ultimately, additional research is needed to predict the downstream
385 consequences of liquefaction across the region.

386 **3.4 Nuances, Uncertainties, and Further Discussion**

387 The three $M_w7.2$ SFZ scenarios used in this study from the BSSC2014 scenario catalog are three
388 interpretations of what a SFZ earthquake could look like. These scenarios originate from the 2008 National
389 Seismic Hazard Map Update (Petersen et al. 2008) and model a $M_w7.2$ rupture on a thrust fault dipping at
390 45 degrees to the south with varying lengths and locations. Other moment magnitudes and fault geometries
391 have been suggested. For example, Black et al. (2023) recently suggested the 923 to 924 AD SFZ rupture
392 may have simultaneously ruptured with the Saddle Mountain fault located in the Olympia Peninsula and
393 the energy released by this dual rupture was estimated at $M_w7.8$. Ultimately, as more SFZ paleoseismic
394 evidence is discovered, dated, and inverted analyzed (e.g., Rasanen and Maurer 2022a,b,c; 2023) better
395 ground motions estimates will arise. Furthermore, physics-based simulations such as Stone et al. (2022)
396 and Frankel and Wirth et al. (2018) are becoming more prevalent and may provide better estimates of
397 ground shaking intensity and uncertainty given they can account for complex effects such as topography
398 and basins. Additionally, as for any liquefaction analysis, site response influences the ground motions. The
399 site response used in this study used empirical site amplification factors based on V_{s30} (e.g., Seyhan and
400 Stewart 2014). More sophisticated analyses such as non-linear site response analysis could be used instead.

401 Nonetheless, the predictions of liquefaction provided herein – based on a regional database of subsurface
402 CPT data and an ensembling of 18 popular liquefaction models – are the most robust presently available.

4.0 Conclusion

403 This study provided a comprehensive forecast of regional liquefaction effects from three $M_w7.2$ SFZ
404 earthquake scenarios by leveraging an ensemble of 18 popular CPT-based liquefaction models. These
405 models were applied to 268 study sites of newly compiled subsurface geotechnical data across the Puget
406 Sound region, resulting in 14,472 individual high-quality liquefaction predictions. Results for all three SFZ
407 scenarios indicate that severe liquefaction is expected in Seattle, WA, and several nearby suburbs,
408 particularly within 20 km of Seattle along the I-5 corridor, where fill and alluvial soils are prevalent.
409 Comparisons with previous studies on the 2001 $M_w6.8$ Nisqually earthquake and a potential $M_w9.0$
410 Cascadia Subduction Zone rupture reveal that SFZ scenarios produce more severe liquefaction within ~20
411 km of Seattle due to higher shaking intensities at the study sites. Additionally, this study assessed the
412 potential for liquefaction-induced shallow foundation damage. Damage is predicted to be relatively
413 common in Seattle and surrounding suburbs, such as Auburn and Issaquah, but more sporadic in locations
414 farther south, like Olympia. The extensive liquefaction and damage predictions made in this study may be
415 useful to aid government agencies and stakeholders in preparing for future SFZ ruptures.

416 Statements and Declarations

417 Data Availability

418 Provided in a supplement is a GIS package containing the predicted probabilities of liquefaction
419 manifestation and foundation damage at 268 study sites. A portion of the CPT data used in this study was
420 funded by the U.S. Geological Survey and are available in Grant et al. (2024). Numerous additional CPTs
421 used were compiled from various partners and sources and are available in Rasanen et al. (2024).

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424 Competing Interests

425 The authors have no relevant financial or non-financial interests to disclose.

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