

Kalman Filter-Based Optimization for Linear Model Predictive Control of Discrete-Time LTI Systems

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Abstract

This paper proposes a novel optimization strategy for Linear Model Predictive Control (MPC) of linear discrete-time systems, in which the classical quadratic programming (QP) or Newton-based update step is replaced by a *Kalman Filter (KF) gain update*. The control input sequence is treated as the state vector of a fictitious dynamical system, and the reference tracking error over the prediction horizon serves as the innovation signal. The Hessian inversion required in the Newton method is replaced by the Joseph-form covariance update, leading to a computationally lightweight and numerically robust algorithm. A formal analogy between the classical penalty parameter λ and the KF tuning parameters q and r is established, showing that $\lambda \approx r/q$, which provides intuitive insight into controller tuning. The steady-state Kalman gain can be computed *offline* via a Riccati iteration, reducing online computation to a single matrix-vector product per time step. The proposed method is validated through simulation on a second-order open-loop unstable discrete-time LTI system under multi-step and sinusoidal reference signals.

Keywords: Model predictive control, Kalman filter, linear discrete-time systems, optimal control, quadratic programming, receding horizon control.

1 Introduction

Model Predictive Control (MPC) is a well-established control strategy widely applied in industrial processes, robotics, and autonomous systems [3, 7, 8]. The fundamental idea is to solve, at each sampling instant, a finite-horizon open-loop optimal control problem using a model of the plant, apply the first element of the resulting optimal input sequence, and repeat the procedure at the next time step following the *receding horizon* principle.

For linear time-invariant (LTI) systems with a quadratic cost function and linear constraints, the MPC problem reduces to a Quadratic Program (QP) [4]. Even in the unconstrained case, the Newton step requires computing \mathbf{H}^{-1} where $\mathbf{H} = 2(M^T M + \lambda L)$. This motivates research into lightweight alternatives, including explicit MPC [2], gradient-based methods [7], and real-time iteration schemes [5].

A parallel line of research has explored connections between optimal control and statistical estimation. The classical duality between the Linear Quadratic Regulator (LQR) and the Kalman Filter (KF) is well known [1]. Inspired by this connection, the present paper investigates whether the same principle can be applied to MPC: treating the control input sequence \mathbf{U} as the state of a fictitious system and using the KF update equations to minimize the tracking cost.

The remainder of this paper is organized as follows. Section 2 defines the system and MPC problem. Section 3 presents the proposed KF-based update, establishes the analogy with the Newton method, and describes the steady-state implementation. Section 4 presents simulation results, and Section 5 concludes the paper.

2 Problem Formulation

2.1 System Description

Consider a linear discrete-time time-invariant system of the form

$$\mathbf{x}[n+1] = A\mathbf{x}[n] + \mathbf{b}u[n], \quad (1)$$

$$y[n] = \mathbf{c}^\top \mathbf{x}[n], \quad (2)$$

where $\mathbf{x}[n] \in \mathbb{R}^{n_x}$ is the state vector, $u[n] \in \mathbb{R}$ is the scalar control input, $y[n] \in \mathbb{R}$ is the scalar output, and $A \in \mathbb{R}^{n_x \times n_x}$, $\mathbf{b} \in \mathbb{R}^{n_x}$, $\mathbf{c} \in \mathbb{R}^{n_x}$ are the system matrices.

2.2 MPC Cost Function

At each time step n , the optimization is performed over prediction horizon K_y and control horizon K_u with $K_u \leq K_y$. For $k > K_u$, the control input is held constant: $u[n+k] = u[n+K_u]$. The control sequence to be optimized is

$$\mathbf{U} = [u[n+1], u[n+2], \dots, u[n+K_u]]^\top \in \mathbb{R}^{K_u+1}. \quad (3)$$

The MPC cost function minimized at each time step is

$$J(\mathbf{U}) = \sum_{k=1}^{K_y} (\tilde{y}_{\text{ref}}[n+k] - \hat{y}[n+k])^2 + \lambda \sum_{k=1}^{K_u} (u[n+k] - u[n+k-1])^2, \quad (4)$$

where $\hat{y}[n+k]$ denotes the predicted output at step k and $\lambda \geq 0$ penalizes rapid changes in the control input.

3 Prediction Formulation and Proposed Method

3.1 Compact Prediction Form

By iterating (1)–(2) forward from the current state $\mathbf{x}[n]$, the vector of predicted outputs $\hat{\mathbf{y}} \in \mathbb{R}^{K_y}$ can be written in compact form as

$$\hat{\mathbf{y}} = Z\mathbf{x}[n] + M\mathbf{U}, \quad (5)$$

where the *free-response matrix* $Z \in \mathbb{R}^{K_y \times n_x}$ and *forced-response matrix* $M \in \mathbb{R}^{K_y \times (K_u + 1)}$ are defined, respectively, as

$$Z = [\mathbf{c}^\top A, \mathbf{c}^\top A^2, \dots, \mathbf{c}^\top A^{K_y}]^\top, \quad (6)$$

$$M(i, j) = \begin{cases} \mathbf{c}^\top A^{i-j} \mathbf{b} & \text{if } j \leq i, \\ 0 & \text{if } j > i, \end{cases} \quad (7)$$

with the last column of M accumulating contributions of the held input for $k > K_u$. Since A , \mathbf{b} , \mathbf{c} are constant, both Z and M are computed *offline*. The penalty term $\lambda \mathbf{U}^\top L \mathbf{U}$ uses the symmetric tridiagonal matrix

$$L = \text{tridiag}(-1, 2, -1), \quad L(K_u + 1, K_u + 1) = 1. \quad (8)$$

3.2 Newton-Based Solution

Substituting (5) into (4), the cost is a strictly convex quadratic in \mathbf{U} . The gradient and Hessian are

$$\nabla J = -2M^\top (\tilde{\mathbf{y}}_{\text{ref}} - Z\mathbf{x}[n] - M\mathbf{U}) + 2\lambda L\mathbf{U} - 2\lambda u_{\text{prev}} \mathbf{e}_1, \quad (9)$$

$$\mathbf{H} = 2(M^\top M + \lambda L), \quad (10)$$

where $u_{\text{prev}} = u[n]$ and $\mathbf{e}_1 = [1, 0, \dots, 0]^\top$. Since \mathbf{H} is positive definite, the unique global minimum is obtained in a *single Newton step*:

$$\delta \mathbf{U} = -\frac{1}{2} \mathbf{H}^{-1} \nabla J = -(M^\top M + \lambda L)^{-1} \nabla J / 2. \quad (11)$$

Since \mathbf{H} depends only on M , L , and λ —all constant—the inverse \mathbf{H}^{-1} is computed once offline, and the dominant online cost is a single matrix-vector product.

3.3 Proposed Kalman Filter Update

The control sequence \mathbf{U} is interpreted as the state of a fictitious system with identity transition dynamics. The tracking error

$$\mathbf{e} = \tilde{\mathbf{y}}_{\text{ref}} - Z\mathbf{x}[n] - M\mathbf{U} \quad (12)$$

serves as the innovation signal. The fictitious measurement model is $\mathbf{e} = -M \delta \mathbf{U} + \mathbf{v}$, $\mathbf{v} \sim \mathcal{N}(\mathbf{0}, rI_{K_y})$, and the process model is $\mathbf{U} \leftarrow \mathbf{U} + \mathbf{w}$, $\mathbf{w} \sim \mathcal{N}(\mathbf{0}, qI_{K_u+1})$. The standard KF equations yield:

$$P_{\text{pred}} = P + qI_{K_u+1}, \quad (13)$$

$$S = M P_{\text{pred}} M^\top + rI_{K_y}, \quad (14)$$

$$K = P_{\text{pred}} M^\top S^{-1}, \quad (15)$$

$$\mathbf{U} \leftarrow \mathbf{U} + K\mathbf{e}, \quad (16)$$

$$P \leftarrow (I - KM) P_{\text{pred}} (I - KM)^\top + KrK^\top. \quad (17)$$

The *Joseph form* (17) ensures that P remains symmetric and positive definite regardless of numerical errors, which is critical for long-running simulations.

3.4 Analogy: $\lambda \leftrightarrow r/q$

At steady state, the Riccati recursion (13)–(17) converges to a fixed point P_{ss} , and the steady-state gain is

$$K_{ss} = P_{ss} M^\top (M P_{ss} M^\top + r I)^{-1}. \quad (18)$$

Comparing with the Newton step (11), for the isotropic case $L = I$ and $P_{ss} = \sigma I$, the Woodbury matrix identity gives

$$\boxed{\lambda \approx \frac{r}{q}}. \quad (19)$$

This result reveals that the ratio r/q plays the same role as the penalty parameter λ in standard MPC: a large r/q produces a small Kalman gain and conservative (smooth) control updates, whereas a small r/q produces an aggressive update. The analogy provides an intuitive interpretation of the KF tuning parameters in terms of familiar MPC design concepts.

3.5 Implementation

Since $H_{kf} = M$ is constant, the Riccati recursion converges to a fixed point satisfying

$$\|P_{ss}^{(k+1)} - P_{ss}^{(k)}\|_F < \varepsilon. \quad (20)$$

Once K_{ss} is available, online computation reduces to a single matrix-vector product $K_{ss} \times \mathbf{e}$ per time step.

3.6 Complete Algorithm

Algorithm 1 KF-Based Linear MPC

Offline phase:

1: Compute prediction matrices M and Z .

Online phase (at each time step n):

2: Measure (or estimate) current state $\mathbf{x}[n]$.

3: Compute prediction: $\hat{\mathbf{y}} = Z\mathbf{x}[n] + M\mathbf{U}$.

4: Compute innovation: $\mathbf{e} = \tilde{\mathbf{y}}_{\text{ref}}(n : n + K_y - 1) - \hat{\mathbf{y}}$.

5: Iterate (13)–(17) until convergence \rightarrow obtain K_{ss} .

6: Update: $\mathbf{U} \leftarrow \mathbf{U} + K_{ss} \mathbf{e}$.

7: Apply saturation: $\mathbf{U} \leftarrow \text{clip}(\mathbf{U}, u_{\min}, u_{\max})$.

8: Compute $\alpha = \min(1, \Delta u_{\max} / \max |\Delta \mathbf{U}|)$; set $\mathbf{U} \leftarrow \alpha \mathbf{U}$.

9: Apply $u[n + 1]$ to the plant.

10: Warm-start: $\mathbf{U} \leftarrow [U(2 : \text{end}); U(\text{end})]$.

4 Simulation Results

4.1 System and Parameters

The proposed method is validated on a second-order open-loop unstable linear discrete-time system:

$$A = \begin{bmatrix} 1.1 & 0.6 \\ 0.2 & 0.1 \end{bmatrix}, \quad \mathbf{b} = \begin{bmatrix} 1 \\ 0 \end{bmatrix}, \quad \mathbf{c} = \begin{bmatrix} 1 \\ 1 \end{bmatrix}. \quad (21)$$

The eigenvalues of A lie outside the unit circle, confirming open-loop instability. Simulation parameters are listed in Table 1.

Table 1: Simulation parameters.

Parameter	Symbol	Value
Sampling time	T_s	0.1 s
Simulation duration	T	40 s
Prediction horizon	K_y	10
Control horizon	K_u	5
Input lower bound	u_{\min}	-1
Input upper bound	u_{\max}	+1
Max input rate	Δu_{\max}	0.2
Process noise covariance	q	10^{-2}
Measurement noise covariance	r	10^{-1}
Initial covariance	p_0	1.0

4.2 Reference Signals

Two reference profiles are combined. The first half ($t \in [0, 20]$ s) uses a multi-step signal:

$$\tilde{y}_{\text{step}}[n] = \begin{cases} 0.4 & n \in [1, 50], \\ 0.8 & n \in [51, 100], \\ 1.2 & n \in [101, 150], \\ 0.8 & n \in [151, 200]. \end{cases} \quad (22)$$

The second half ($t \in (20, 40]$ s) uses a sinusoidal signal:

$$\tilde{y}_{\text{sin}}[n] = 0.8 + 0.3 \sin(0.5\pi(n - 200)T_s). \quad (23)$$

4.3 Results and Discussion

The simulation results confirm stable and accurate reference tracking across both reference profiles. During the multi-step phase, the controller successfully performs step transitions while respecting the input rate constraint $|\Delta u| \leq 0.2$ and the saturation limits $u \in [-1, 1]$. During the sinusoidal phase, the controller tracks the reference with small steady-state error, demonstrating the ability to handle smooth time-varying signals.

The tuning ratio $r/q = 10$, corresponding to $\lambda \approx 0.1$ via the analogy (19), produces smooth control actions with moderate tracking bandwidth. Increasing q (equivalently decreasing λ) leads to more aggressive updates and faster tracking at the cost of larger input excursions, consistent with classical MPC behavior.

Table 2 compares the average online computation cost.

5 Conclusions

This paper has presented a Kalman Filter-based optimization strategy for linear discrete-time Model Predictive Control. The following conclusions are drawn:

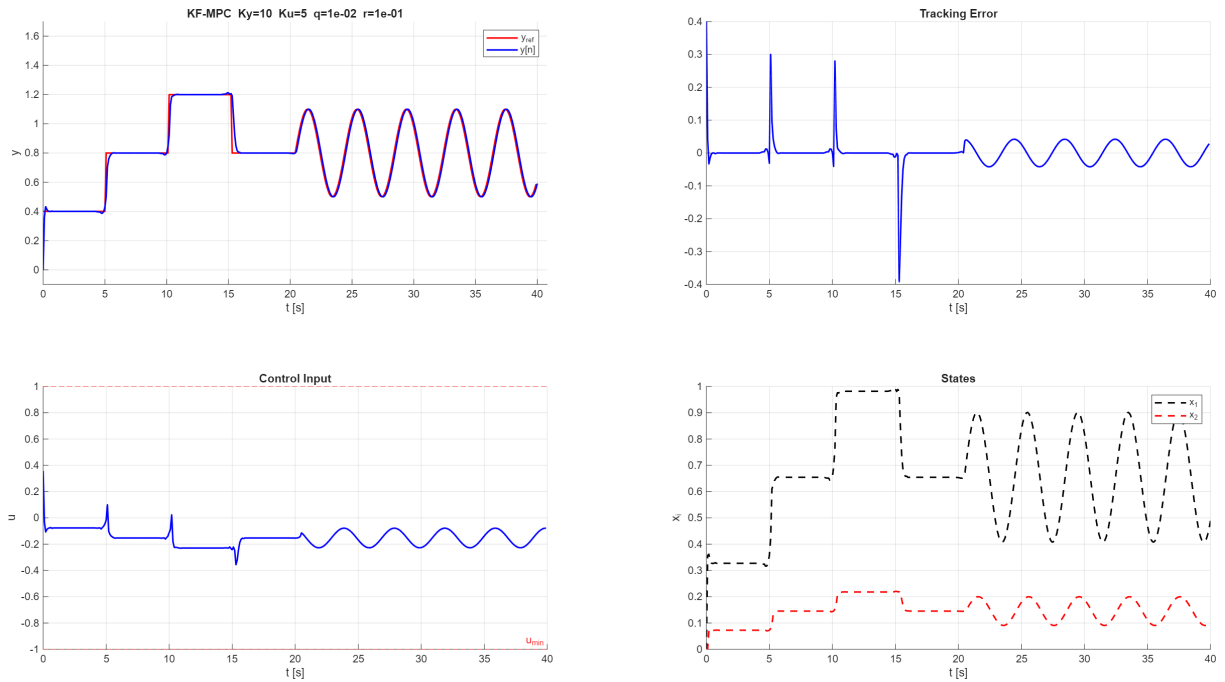


Figure 1: Simulation results for the proposed KF-MPC ($K_y = 10$, $K_u = 5$, $q = 10^{-2}$, $r = 10^{-1}$). Top-left: reference tracking. Top-right: tracking error. Bottom-left: control input with saturation limits. Bottom-right: system states x_1 and x_2 .

Table 2: Average online computation cost per time step.

Method	Online operations	Relative cost
Newton-based MPC	$\mathbf{H}^{-1} \times \nabla J$	$1 \times$ (baseline)
KF-MPC (online P)	Riccati + $K \times \mathbf{e}$	$\approx 1.2 \times$
KF-MPC (steady-state)	$K_{ss} \times \mathbf{e}$	$\approx 0.3 \times$

1. The proposed KF-MPC is algebraically equivalent to the Newton solution of the unconstrained MPC problem. In the steady-state case, both reduce to a single matrix-vector multiplication per time step.
2. A formal analogy $\lambda \approx r/q$ bridges MPC design practice and probabilistic estimation theory, providing an intuitive interpretation of the KF tuning parameters.
3. The Joseph-form covariance update ensures numerical stability and positive definiteness of P throughout the simulation.
4. Simulation results on an open-loop unstable second-order system confirm stable tracking under input saturation and rate constraints for both step and sinusoidal reference signals.

Code Availability

The MATLAB implementation of the proposed KF-MPC algorithm is publicly available at:

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