

# A numerical procedure based on the Backward Euler method for two point boundary value ordinary differential equation (ODE) systems with applications to a model in flight mechanics

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## Abstract

This short communication develops a numerical procedure suitable for a large class of ordinary differential equation systems found in models in physics and engineering. More specifically, we have utilized the standard Backward Euler method combined with a MAT-LAB function for obtaining a method suitable for a class of two point boundary value ODE non-linear systems. In the last section, we apply the method to a model in flight mechanics.

Keywords: Two point boundary value ODE system, Backward Euler method, model in flight mechanics.

MSC: 65L10, 65L12

## 1 Introduction

In this article we develop an application of the Backward Euler method adapted for a two point boundary value ODE (ordinary differential equation) system to a model in flight mechanics.

The model in flight mechanics here addressed may be found in [1].

Details on the Sobolev spaces involved may be found in [2].

Related results to those concerning the generalized method of lines, may be found in the here referenced books of 2011 and 2020, [3, 4] respectively.

For a reference on standard finite differences schemes, please see [5].

Finally, related results concerning the fourth order Runge-Kutta method have been presented in [6].

## 2 The main numerical method

Consider the first order system of ordinary differential equations given by

$$\frac{du_j}{dt} = f_j(\{u_l\}), \text{ on } [0, t_f] \forall j \in \{1, 2, 3\},$$

with the boundary conditions

$$u_1(0) = 0, \quad u_1(t_f) = u_f = 11000.$$

Here  $\mathbf{u} = \{u_l\} \in W^{1,2}([0, t_f], \mathbb{R}^3)$  and  $f_j$  are functions at least of  $C^1$  class,  $\forall j \in \{1, 2, 3\}$ .

Concerning a finite differences scheme, we denote the number of nodes on  $[0, t_f]$  by  $m_8$  and set  $d = t_f/m_8$ .

Based on the Backward Euler method, we propose the following algorithm.

In finite differences, (indeed we have made it through an appropriate MAT-LAB function), we define  $t_f = t_0$  (here  $t_0$ , the final time, it is also a unknown variable to be minimized through the minimization of the functional  $J$  to be specified in the next lines),

$$u_1(0) = 0, \quad u_2(0) = G_0, \quad u_3(0) = V_0;$$

Fixing  $k_{10} = 15$ ,  $m_8 = 10000$ ,  $d = m_8/t_f = m_8/t_0$  we calculate  $(u_1)_1, (u_2)_1$  and  $(u_3)_1$  through the following iterations,

$$\text{Set } (u_{01})_1 = u_1(0), \quad (u_{02})_1 = u_2(0), \quad (u_{03})_1 = u_3(0).$$

For  $k_3$  from 1 to  $k_{10}$  do

1.  $(u_j)_1 = u_j(0) + f_j((u_{01})_1, (u_{02})_1, (u_{03})_1) d, \quad \forall j \in \{1, 2, 3\},$
  2.  $(u_{0j})_1 = (u_j)_1, \quad \forall j = \{1, 2, 3\}.$
- end;

for  $k$  from 2 to  $m_8$  do

$$(u_{0j})_k = (u_j)_{k-1}, \quad \forall j \in \{1, 2, 3\}.$$

for  $k_3$  from 1 to  $k_{10}$  do

1.  $(u_j)_k = (u_j)_{k-1} + f_j((u_{01})_k, (u_{02})_k, (u_{03})_k) d, \quad \forall j \in \{1, 2, 3\},$
  2.  $(u_{0j})_k = (u_j)_k, \quad \forall j = \{1, 2, 3\}.$
- end;

end;

Finally, having obtained

$$\{(u_j)_k(G_0, V_0, t_0)\},$$

we obtain  $(G_0, V_0, t_0)$  by minimizing the functional

$$J(G_0, V_0, t_0).$$

where

$$\begin{aligned}
J(G_0, V_0, t_0) &= 25^2 t_0^2 + 30^2 ((u_1)_{m_8}(G_0, V_0, t_0) - 11000)^2 + (u_2)_{m_8}(G_0, V_0, t_0) \\
&\quad + 500^2 \sum_{j=1}^{m_8-2} \left( \frac{((u_1)_{j+2} - 2(u_1)_{j+1} + (u_1)_j)}{d^2} \right)^2.
\end{aligned} \tag{1}$$

**Remark 2.1.** *Through the minimization of such a functional  $J$ , we intend to obtain  $(G_0, V_0, t_0) \in \mathbb{R}^3$  which minimizes the final time  $t_f = t_0$  and approximately satisfy the boundary conditions  $u_1(t_f = t_0) = 11000$ ,  $u_2(t_f = t_0) = 0$  and, at the same time, minimizes the integral of the second derivative square of  $u_1$  (intending to minimize the trajectory curvature as well) along the time interval  $[0, t_f]$ .*

The problem is then approximately solved.

### 3 Applications to a flight mechanics model

We present numerical results for the following system of equations, which models the in plane climbing motion of an airplane (please, see more details in [1]).

$$\begin{cases} \dot{h} = V \sin \gamma, \\ \dot{\gamma} = \frac{1}{m_f V} (F \sin[a + a_F] + L) - \frac{g}{V} \cos \gamma, \\ \dot{V} = \frac{1}{m_f} (F \cos[a + a_F]) - D - g \sin \gamma \\ \dot{x} = V \cos \gamma, \end{cases} \tag{2}$$

with the boundary conditions,

$$\begin{cases} h(0) = h_0, \\ \gamma(0) = \gamma_0 \\ x(0) = x_0 \\ h(t_f) = h_f, \end{cases} \tag{3}$$

where the optimal final time  $t_f = t_0$  will be also calculated,  $h$  is the airplane altitude,  $V$  is its speed,  $\gamma$  is the angle between its velocity and the horizontal axis, and finally  $x$  denotes the horizontal coordinate position.

For numerical purposes, we assume (data close to those of an Air bus 320)

$$m_f = 120,000 \text{ Kg}, S_f = 260 \text{ m}^2, a = 0.138 \text{ rad}, g = 9.8 \text{ m/s}^2,$$

$$\rho(h) = 1.225(1 - 0.0065h/288.15)^{4.225} \text{ Kg/m}^3,$$

$$a_F = 0.0175,$$

$$(C_L)_a = 5$$

$$(C_D)_0 = 0.0175,$$

$$K_1 = 0.0,$$

$$K_2 = 0.06$$

$$(C_L)_0 = 0,$$

$$\begin{aligned}
C_D &= (C_D)_0 + K_1 C_L + K_2 C_L^2, \\
C_L &= (C_L)_0 + (C_L)_a a, \\
L &= \frac{1}{2} \rho(h) V^2 C_L S_f, \\
D &= \frac{1}{2} \rho(h) V^2 C_D S_f, \\
F &= 240000
\end{aligned}$$

and where units refer to the International System.

To simplify the analysis, we redefine the variables as below indicated:

$$\begin{cases} h = u_1, \\ \gamma = u_2 \\ V = u_3 \\ x = u_4. \end{cases} \quad (4)$$

Thus, denoting  $\mathbf{u} = (u_1, u_2, u_3, u_4) \in U = W^{1,2}([0, t_f]; \mathbb{R}^4)$ , the system above indicated may be expressed by

$$\begin{cases} \dot{u}_1 = f_1(\mathbf{u}) \\ \dot{u}_2 = f_2(\mathbf{u}) \\ \dot{u}_3 = f_3(\mathbf{u}) \\ \dot{u}_4 = f_4(\mathbf{u}), \end{cases} \quad (5)$$

where,

$$\begin{cases} f_1(\mathbf{u}) = u_3 \sin(u_2), \\ f_2(\mathbf{u}) = \frac{1}{m_f u_3} (F \sin[a + a_F] + L(\mathbf{u})) - \frac{g}{u_3} \cos(u_2), \\ f_3(\mathbf{u}) = \frac{1}{m_f} (F \cos[a + a_F] - D(\mathbf{u})) - g \sin(u_2) \\ f_4(\mathbf{u}) = u_3 \cos(u_2). \end{cases} \quad (6)$$

We solve this last system for the following boundary conditions:

$$\begin{cases} h(0) = 0 \text{ m}, \\ x(0) = 0 \text{ m}, \\ h(t_f) = 11000 \text{ m}. \end{cases} \quad (7)$$

Observe that having calculated a solution  $(h, \gamma, V)$  we may easily calculate  $x$  through the fourth equation, that is,

$$x(t) = x(0) + \int_0^t V(t) \cos(\gamma(t)) dt$$

Thus, for a solution, we may consider just the first three equations in the three variables  $(h, \gamma, V)$ . We have numerically obtained  $t_f = t_0 = 662.9544s$  and for the solutions for  $h, \gamma, V$ , please see the figures 1, 2 and 3, respectively. We have set  $m_8 = 10000$  nodes.

Here we present the software in MAT-LAB entitled "FlightMech08Sept2026A" through which such numerical results have been obtained.

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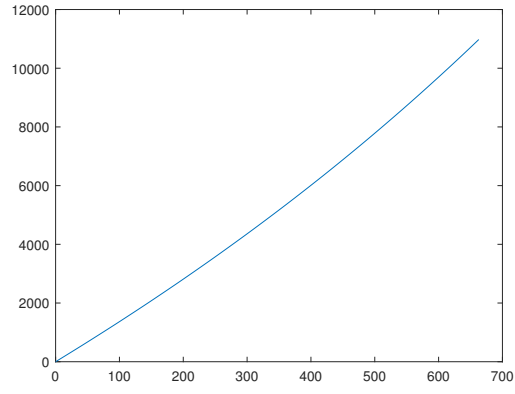


Figure 1: The solution  $h$  (in m) for  $t_f = 662.9544s$ .

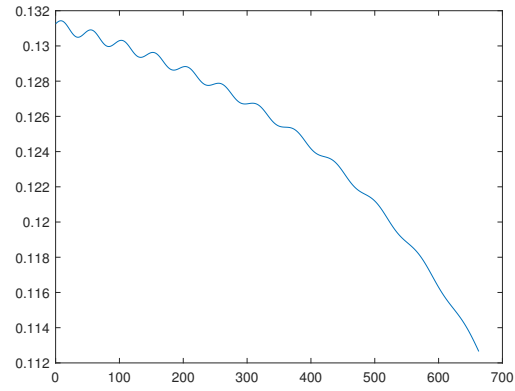


Figure 2: The solution  $\gamma$  (in rad) for  $t_f = 662.9544s$ .

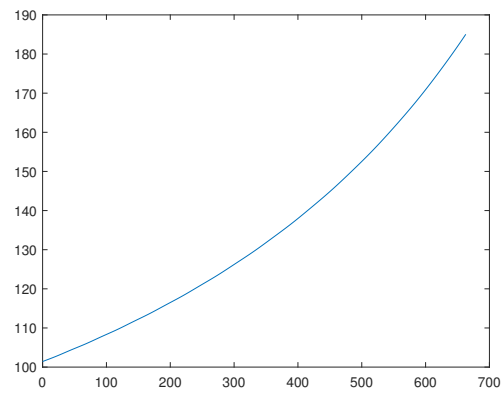


Figure 3: The solution  $V$  (in m/s) for  $t_f = 662.9544s$ .

```

1. clear all global m8 d tf CL CD ho go vo Sf mf a aF F h v g W5 G K8 b25 k10 to
   m8=10000;
   K8=0;
   mf=120000;
   Sf=260;
   G=9.81;
   a=0.138;
   aF=0.0175;
   F=240000;
   k10=10;
   CLa=5;
   CDo=0.0175;K1=0.0;
   K2=0.06;
   CLo=0;
   CL=CLo+CLa*a;
    $CD = CDo + K1 * CL + K2 * CL^2$ ;
   lb(1,1)=70;
   ub(1,1)=310;
   lb(2,1)=0.05;
   ub(2,1)=0.45;
   lb(3,1)=450;
   ub(3,1)=800;
   xo(1,1)=120;
   xo(2,1)=0.15;
   xo(3,1)=670;
   b14=1;
   k3=1;
   while (b14 > 10-4) && (k3 < 5)
   k3
   k3=k3+1;
   k10=k10+5;
   b12=1;
   k1=1;
   while (b12 > 10-3.2) && (k1 < 10)
   k1
   k3
   k1=k1+1;
   X=lsqnonlin('funFlightMech08Sept2026A',xo,lb,ub);
   b12=max(abs(X-xo));

```

```

xo=X;
h(m8/2,1);
end;
b14=max(abs(b25));
end;
for i=1:m8
x8(i,1)=i*d;
end;
plot(x8,h)

```

\*\*\*\*\*

With the main function entitled "funFlightMech08Sept2026A"

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```

1. function W5=funFlightMech08Sept2026A(x)
    global m8 d tf CL CD ho go vo Sf mf a aF F h v g W5 G K8 k10 b25 to
    Ho(1,1)=0;
    Vo(1,1)=x(1,1);
    Go(1,1)=x(2,1);
    to=x(3,1);
    d=to/m8;
    ho(1,1)=0;
    vo(1,1)=120;
    go(1,1)=0.15;
    k=1;
    for k5=1:k10
         $r(k) = abs(1.225 * (1 - 0.0065 * Ho(1,1)/288.15)^{4.225});$ 
         $L = 1/2 * r(k) * vo(1,1)^2 * CL * Sf;$ 
         $D = 1/2 * r(k) * vo(1,1)^2 * CD * Sf;$ 
        h(k,1)=(Ho(1,1)+vo(k,1)*sin(go(k,1))*d+K8*ho(k,1)*d)/(1+K8*d);
        g(k,1)=(Go(1,1)+1/mf*(F*sin(a+aF)+L)/vo(k,1)*d-G/vo(k,1)*cos(go(k,1))*d+K8*go(k,1)*d)/(1+K8*d);
        v(k,1)=(Vo(1,1)+1/mf*(F*cos(a+aF)-D)*d-G*sin(go(k,1))*d+K8*vo(k,1)*d)/(1+K8*d);
        b25(k,1)=abs(v(k,1)-vo(k,1));
        vo(k,1)=v(k,1);
        ho(k,1)=h(k,1);
        go(k,1)=g(k,1);
    end;
    for k=2:m8
        vo(k,1)=v(k-1,1);
        ho(k,1)=h(k-1,1);
        go(k,1)=g(k-1,1);
    end;

```

```

for k5=1:k10
r(k) = abs(1.225 * (1 - 0.0065 * ho(k, 1)/288.15)^(4.225));
L = 1/2 * r(k) * vo(k, 1)^2 * CL * Sf;
D = 1/2 * r(k) * vo(k, 1)^2 * CD * Sf;
h(k,1)=(h(k-1,1)+vo(k,1)*sin(go(k,1))*d+K8*ho(k,1)*d)/(1+K8*d);
g(k,1)=(g(k-1,1)+1/mf*(F*sin(a+aF)+L)/vo(k,1)*d-G/vo(k,1)*cos(go(k,1))*d+K8*go(k,1)*d)/(1+K8*d);
v(k,1)=(v(k-1,1)+1/mf*(F*cos(a+aF)-D)*d-G*sin(go(k,1))*d+K8*vo(k,1)*d)/(1+K8*d);
b25(k,1)=abs(v(k,1)-vo(k,1));
vo(k,1)=v(k,1);
ho(k,1)=h(k,1);
go(k,1)=g(k,1);
end;
end;
W5(1,1)=30*(h(m8,1)-11000);
W5(2,1)=g(m8,1);
W5(3,1)=25*to;
for i=1:m8-2
W5(i + 3, 1) = 500 * (h(i + 2, 1) - 2 * h(i + 1, 1) + h(i, 1))/d^2;
end;
*****

```

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## 5 Conclusion

In this article we have presented a numerical procedure for solving a class of two point boundary value ODE systems with applications to a flight mechanics model.

The numerical method is based on the Backward Euler approach adapted for a two point boundary value ODE system.

In a near future research we intend to address some other linear and non-linear cases.

1. **Conflict of interest declaration:** The author declares no conflict of interest concerning this article.



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